

OTIC FILE CORY AFATL-TR-87-10



## AD-A182 728

User Instructions for the EPIC-3 Code

G R Johnson R A Stryk

HONEYWELL INCORPORATED
DEFENSE SYSTEMS DIVISION
7225 NORTHLAND DRIVE
BROOKLYN PARK, MINNESOTA 55428

**MAY 1987** 

FINAL REPORT FOR PERIOD OCTOBER 1983 - APRIL 1987

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED



AIR FORCE ARMAMENT LABORATORY

Air Force Systems Command United States Air Force Eglin Air Force Base, Florida

#### NOTICE

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report has been reviewed by the Public Affairs Office (PA) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

Marlin Diesence.

MARTIN F. ZIMMER

Technical Director, Munitions Division

Even though this report may contain special release rights held by the controlling office, please do not request copies from the Air Force Armament Laboratory. If you qualify as a recipient, release approval will be obtained from the originating activity by DTIC. Address your request for additional copies to:

Defense Technical Information Center Cameron Station Alexandria, Virginia 22304-6145

If your address has changed, if you wish to be removed from our mailing list, or if the addressee is no longer employed by your organization, please notify AFATL/ MNW, Eglin AFB FL 32542-5434.

Copies of this report should not be returned unless return is required by security considerations, contractual obligations, or notice on a specific document.

SECLIFITY CL	ASSET KATEN	OF THEE PAGE

				REPORT DOCU	MENTATION	PAGE		
14. REPORT	SECURITY CLASSIFIC	CATION			16. RESTRICTIVE	MARKINGS		
Unclassified					NA			
2a. SECURITY CLASSIFICATION AUTHORITY					1	AVAILABILITY OF REPO		
<u>NA</u>						d for public rel	ease; distribu	tion
29. DECLASSIFICATION/DOWNGRADING SCHEDULE					unlimited	,		
NA			-		4 140147001410	RGANIZATION REPORT		
4. PERFORM	NG ORGANIZATION I	HEPORT	NUMBER(5)		1	TR-87-10	MONMET(0)	
	PERFORMING ORGA	ANIZATIO	W	So. OFFICE SYMBOL		ITORING ORGANIZATIO	ON .	
Hone	ywell Inc.			(If applicable)	Air Force	e Armament L	aboratory (M	INW)
6c. ADORESS	(City, State, and ZIP C	(ode)			7c. ADORESS (Ch)	, State, and ZIP Code)		<del></del>
Defen	se Systems D	Divisio	n					
	Northland D				Eglin AF	B, Florida 325	42	
	dyn Park, M							
	runding/sponsor			8b. OFFICE SYMBOL (# applicable)		I INSTRUMENT IDENTIF		
DARI	PA		ao and	(MNW)		3-C-0506 and	F8635-85-C-	0097
Sc. ADDRESS	(City, State, and ZIP C	iade)			10. SOURCE OF FI		Tana	
Ealin	AED Elorida	225	42		ELEMENT NO.	PROJECT NO.	TASK NO	WORK UNIT ACCESSION NO
Egun	AFB, Florida	4 323	42		2502	07	04	
11 TITLE (Inc.	ude Security Classifics	ndoni					1 04	
Users	Instructions	for th	e EPIC-3	Code (U)				
12. PERSONA	N. AUTHOR(8)	-		<u> </u>		<del></del>		
G.R.	Johnson and	R.A.	Stryk					
13s TYPE OF	REPORT		13b. TIME CO		14. DATE OF REPORT (Year, Month, Day) 18. PAGE COUNT			
Fina	1		FROM 1	<u>0/83</u> то <u>4/87</u>	May	1987	77	
16. SUPPLEM	ENTARY NOTATION							
				18. SUBJECT TERMS (Cont	·			<del></del>
17.	COSATI COO						-	
FIELD	GROUP	506	GROUP	NABOR Node Tetrahedral Ele			nent Code mputations	
	<del></del>	-		Eroding Interfa		impact oo	patatorio	
19 ABSTRACT	T (Continue on reverse	I necess	ery and identify by	block number)		·		<del>"</del>
code are material of the E. An exam	a NABOR of data library, PIC-2 code. Inple problem	ption a targ Instru is also	for variab get drop/ac ctions are o provided		rity, eroding in er changes to Preprocessor, t	nterfaces, impromake it more he Main Routi	oved material similar to the length of the l	models, a 1986 version
	SIFIED/UNLIMITED		SAME AS P	PT. DTIC USERS	Unclassifie	<del></del>	<del></del>	ZZe OFFICE SYMBOL
	Dennis May				(904) 882		ĺ.	
	,							MNW

### **PREFACE**

This report on the EPIC-3 computer code was prepared by Honeywell Inc., Defense Systems Division, 7225 Northland Drive, Brooklyn Park, Minnesota 55428, for the U.S. Air Force Armament Laboratory, Eglin Air Force Base, Florida 32542, under Contracts F08635-83-C-0506 and F08635-85-C-0097.

This effort was conducted during the period from October 1983 to April 1987. The authors would like to thank Mr. Mike Gunger, Lt. Dennis L. May, and Lt. Paul L. Thee, AFATL/MNW program managers, and William H. Cook, AFATL/MNW, for many helpful technical discussions.

Some improvements in the data handling routines and anisotropic material algorithms were funded by the Ballistic Research Laboratory under another contract.

Acces	sion Fo	r						
NTIS	GRA&I							
DTIC :	PAB	1						
Unannounced 🔲								
Justi	ficatio	on						
	Distribution/ Availability Codes							
	Avail							
Dist	Spec	•						
A-1								



## **TABLE OF CONTENTS**

Sect	ion	Page
I	INTRODUCTION	1
II	USER INSTRUCTIONS	2
	1. Input Data for the Proprocessor a. Material Descriptions b. Node Geometry c. Element Geometry 2. Input Data for the Main Routine 3. Input Data for the Postprocessor a. State Plots b. Time Plots 4. Programs Structure and File Designation 5. Options for Memory Containment of Data 6. Instructions for Changing Program Dimensions 7. Example Problem	25 37 41 49 53 60 64 66 69 73
Ш	CONCLUSIONS AND RECOMMENDATIONS	78
	REFERENCES	70

## LIST OF ILLUSTRATIONS

Figure		Page
1a	Preprocessor Input Data	3
1b	Preprocessor Input Data	4
2	Material Input Data	5
3a	Node Input Data	6
<b>3</b> b	Node Input Data	7
4	Element Input Data	8
5a	Main Routine Input Data	9
5b	Main Routine Input Data	10
6	Postprocessor Input Data for State Plots	11
7	Postprocessor Input Data for Time Plots	12
8	Nodal Spacing for Various Expansion Factors	13
9	Arrangement of Six Tetrahedra into a Composite Brick Element	14
10	Node/Element Input Data Example	15
11	Rod Shape Geometry	16
12	Nose Shape Geometry	17
13	Flat Plate Geometry	18
14	NABOR Filled Plate Node Geometry	19
15	NABOR Node Geometry	20
16	Summary of Nodes and Elements in Various Shapes	21
17	Master Surface Options for Sliding Interfaces	22
18	Pressure Model for Crushable Solids. Specific Data Shown are for Concrete	23
19	Euler Angles for Principal Material Axes X', Y', Z' Relative to Initial System Axes X, Y, Z	24
20	Sign Convention for Internal Loads	24
21	Hierarchy Chart for the Preprocessor	70
22	Hierarchy Chart for the Main Routine	71
23	Hierarchy Chart for the State Plots Postprocessor	72

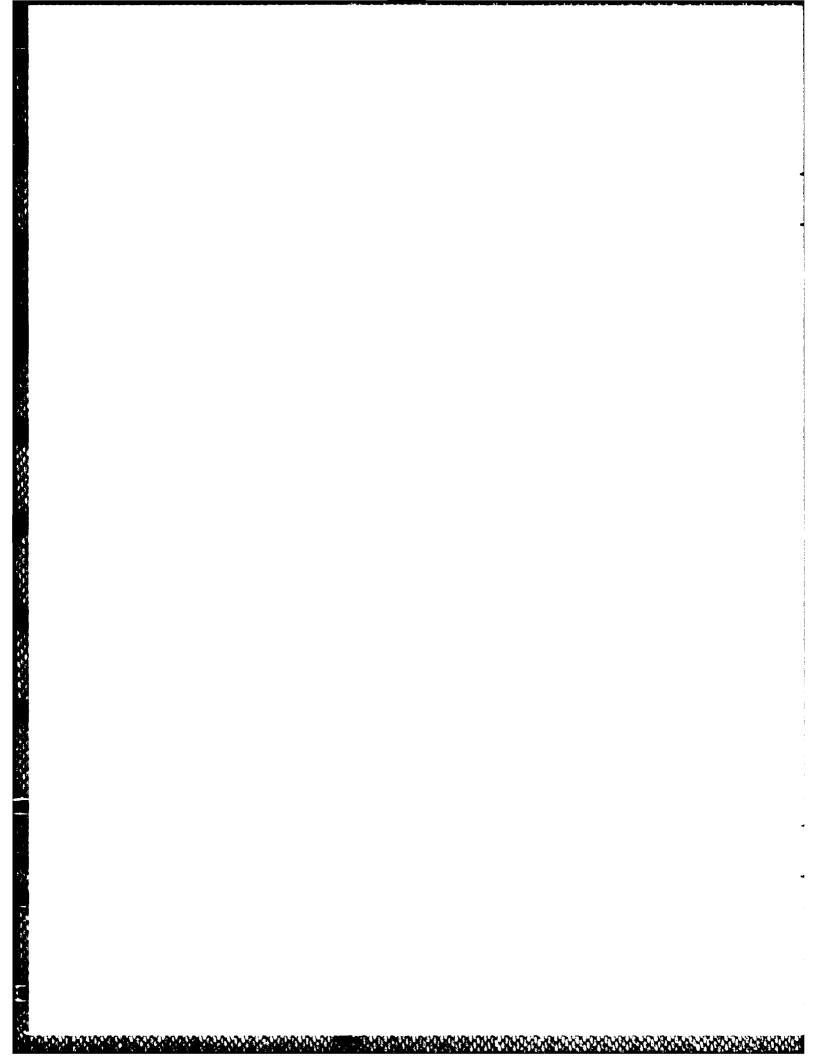
## LIST OF ILLUSTRATIONS (concluded)

Hierarchy Chart for the Time Plots Postprocessor	73
Input Data for the Example Problem	75
Computed Response of Example Problem	76
Output Data for the Example Problem	77
	Input Data for the Example Problem

## LIST OF TABLES

<b>Fable</b>		Page
1	Subroutine Groupings for the EPIC-3 Code	67
2	Required Groups of Subroutines for Various Types of Runs	68

vii/viii (blank)



# SECTION I

This report provides user instructions for the 1987 version of the three-dimensional EPIC-3 code.

The first documented version of the EPIC-3 code was developed for the Ballistic Research Laboratory (BRL) in 1977 (Reference 1), the second version was developed for the Air Force Armament Laboratory in 1978 (Reference 2), and the third version was developed for the BRL in 1980.

The 1987 version, described in this report, incorporates a NABOR node option for variable nodal connectivity. Other new features are improved material models and a data library, which are consistent with the 1986 version of the EPIC-2 code (Reference 3); eroding interfaces for projectile penetration into thick targets; and a target add option. Numerous other changes have also been incorporated since 1980.

One of the distinguishing features of the EPIC-3 code is that it is primarily based on a tetrahedral element formulation. This allows problems with severe distortions to be run without rezoning. This is a very desirable feature for many intense impulsive loading problems involving high velocity impact or explosive detonation.

The 1987 version of the EPIC-3 code, as well as the user instructions in this report, have been made as similar as possible to the corresponding 1986 version of the EPIC-2 code (Reference 3).

# SECTION II USER INSTRUCTIONS

This section provides user instructions for the EPIC-3 code. The code consists of a Preprocessor, Main Routine, and Postprocessor for state and time plots. The formulation is not provided here; however, most of the equations are identical to those of Reference 2. Some comments concerning the formulation of the current version of the code follow:

- The material strength models for solids and crushable materials are given in References 4 and 5.
- The fracture model for solids is given in Reference 6.
- The average pressure formulation is given in References 7 and 8.
- The sliding interface formulation is given in References 9 and 10.
- The eroding interface formulation is given in Reference 8.
- Examples of anisotropic computations, performed with the 1980 version of the EPIC-3 code, are given in Reference 7.
- The three-dimensional NABOR node formulation will appear in the final report for this contract. The NABOR formulation for plane strain is given in Reference 11.
- A characteristic of tetrahedral elements is that they sometimes produce a pressure field that oscillates spatially. This can cause inaccuracies for cases where the material strength or fracture is dependent on the pressure in the element. This is overcome by computing a nodal pressure which is the average of the element pressures for all elements that contain a specified node. The nodal pressures do not oscillate spatially but rather form a smooth pressure field. A smoothed element pressure is then defined as the average of the four associated nodal pressures. This smoothed pressure is used for the strength and fracture models, which are pressure dependent.

A description of input data for the EPIC-3 code is given in Figures 1 through 20.

DESCRIPTION CARD (A80)
DESCRIPTION OF PROBLEM
MISCELLANEOUS CARD (1415)  CASE PRINT I SAVE INSLID BYZRIG SPLIT I NIR I NNR I NIL I NOR I NIR I NPL I UNIT I NRST ()
CASE PRINT SAVE NSLID XYZRIG SPLIT NIR NNR NIL NOR NIR NPL UNIT NRST
MATERIAL DATA CARDS - DESCRIPTION FOLLOWS
BLANK CARD 1 ENDS MATERIAL DATA
PROJECTILE SCALE / SHIFT / ROTATE CARD (7F10.0)
XSCALE YSCALE ZSCALE XSHIFT ZSHIFT ROTATE SLANT
NODE DATA CARDS FOR PROJECTILE - DESCRIPTION FOLLOWS
BLANK CARD 2 ENDS PROJECTILE NODE DATA
TARGET SCALE / SHIFT / ROTATE CARD (7F10.0)
XSCALE YSCALE ZSCALE XSHIFT ZSHIFT ROTATE SLANT
NODE DATA CARDS FOR TARGET - DESCRIPTION FOLLOWS
BLANK CARD 3 ENDS TARGET NODE DATA
ELEMENT DATA CARDS FOR PROJECTILE - DESCRIPTION FOLLOWS
BLANK CARD 4 PROJECTILE ELEMENT DATA
ELEMENT DATA CARDS FOR TARGET - DESCRIPTION FOLLOWS
BLANK CARD 5 ENDS TARGET ELEMENT DATA
<u></u>
SLIDING SURFACE IDENTIFICATION CARDS - AS REQUIRED (1015, 3F10.0)
MGEOM SEEK IT M1 S1 SN NSN NSG ISR NAB FRICT REFVEL EROOE
MASTER DEFINITION CARD FOR PLATE GEOMETRY (MGEOM = 1) (915)  NML NMW IDL IDW IDIA NBOT NLAST MGNXT MINXT
NML NMM IDE IDM IDM NOOTHEEST IMENTALIMITES.
MAGNET DESCRIPTION OF DO POSE DOD OCCUPATION WAS COME ON ONE
MASTER DEFINITION CARD FOR NOSE-ROD GEOMETRY (MGEOM = 2) (315, 20X, 215)  NOR NIR NPL   NP
THE THE PARTY OF T
MACTED DECIMINAL CARD PAR DICK CECNICIDY (MACECNIA 3) (NE 15Y ME)
MASTER DEFINITION CARD FOR DISK GEOMETRY (MGEOM = 3) (215, 15X, 415)  NRING MCODE
India mood
MASTER DEFINITION CARD FOR CYLINDER GEOMETRY (MGEOM = 4) (4/5,15X,215)
NRING NPL   IDL   MCODE   MCODE   MAGNAT   MINAT   MIN
MASTER DEFINITION CARD FOR GENERAL GEOMETRY (MGEOM = 5) (415)
NBOT NLAST MGNXT MINXT
INDIVIDUAL MASTER SURFACE CARD(S) FOR MGEOM = 5 (7/5)
NCOMP M1 M2 M3 M4 M5 INC
And the second s
SLAVE NODE LIMITS CARD FOR NSN=0 (6F10.0, I5)
XMAX XMIN YMAX YMIN ZMAX ZMIN NBOX
NSG GROUPED SLAVE NODE CARD(S) FOR NSG>0 (315)
SIG SNG NC //////////////////////////////////
INDIVIDUAL SLAVE NODE CARD(S) FOR NSN>0 AND NSG = 0 (1615)
S1   S2

Figure 1a. Preprocessor Input Data

RESTRAI	NED N	IODES IDE	NTIFICA	TION CARD	S - AS REQUIRI	ED (215, 2X, 311)						
	NFG		11111				illilli	111111	THIII.	11111	IIII	VIIII.
		Y	_ px, n	r, IZ								
INDIVIDU	AL RE	STRAINED	NODES	CARDS - FO	OR NFG = 0 (16	15)						
F1	F2					FN	T	T				
	SUPED FNG	RESTRAIL	NED NO	DES CARDS	(315) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)							
DETONAT	TION C	ARD (4F10	1.0)									
XDE	T	YDET		ZDET	TBURN	IIIIII	IIIII		IIIIII	IIII	IIII	* 111112
INITIAL VE	ELOCI	TY CARD (	7F 10.0)									
PXDC	OT	PYDO	T T	PZDOT	TXDOT	TYDOT	T	TZDOT	DT	1	11111	<i>• पागाः</i>

\* INDICATES REQUIRED CARDS - ALL OTHERS OPTIONAL

Figure 1b. Preprocessor Input Data

	AROS FOR SOLI						~~~~~
MATL 0	IDAM IFA	L DFRACE EFA	w/////////////////////////////////////				
S MATERIAL	CARDS FOR SO	I IDC INDUIT DAT	A. 1415 SY ES	0 A40/4/9E10.0V			
MATL 1	IDAM IFA				DESCRIPTION		
	<del></del>						
DENSITY	SPH HEAT	CONDUCT	T ALPHA	TEMP1	TROOM	TMELT	X1
SHEAR MO	O   C1	C2	l N	C3	M	T C4	SMAX
L			<del> </del>				
K1	K2	К3	1 [	T CL	T CQ	PMIN	ТСН
<b></b>							
D1	D2	D3	D4	D5	SPALL	EFMIN	T X2
							<del></del>
MATERIAL CA	ARDS FOR EXPL	OSIVES FROM L	JBRARY (215)				
MATL 0	**********						
3 MATERIAL (	CARDS FOR EXP	LOSIVES INPUT	DATA: (215, 20	X, A48/6F10.0/7F	10.0)		
MATL 2			1	MATERIAL	DESCRIPTION		
DENSITY	ENERGY	DET VEL	CL	CO	СН	IIIIIIII	
C1	C2	СЗ	C4	C5	X1	X2	VIIIIIII
						· <b>-</b>	
MATERIAL CA	ARDS FOR CRUS	HABLE SOLIDS	FROM LIBRARY	(2IS, 15X, F5.0)			
MATL 0	IIIIIIII	EFAI		<i>Millillilli</i>	IIIIIIIII	HIIIIIII	
						٠.	
4 MATERIAL (	CARDS FOR CRI	ISHARI E SOLIO	S INPLIT DATA	215, 15X, F5.0, A	48/3E10 0/2/8E1	0 M1	
MATL 3	IIIIIII	THE EFAI			RIAL DESCRIPT		
<del> </del>			J	··			
DENSITY	SPH HEAT	TEMP1	IIIIIIIX	millioni	ummini.	mmmm	viiiiiiiiii
	··	<del></del>	<i></i>			<i></i>	
SHEAR MOD	C1	T C4	SMAX	T CL	CQ	PMIN	T CH T
	<u> </u>			<u> </u>	1	1 1	<u> </u>
PCRUSH	UCRUSH	T K1	Т к2	К3	KLOCK	I III OCK	<del></del> -
	Conosii				1 RECOR	ULOCK	X1
MATERIAI C	CARRE EOR ANI	EOTROPIC POL	IDC MIDIT DAT	A (415, 5X, F5.0, /			
MATL 4	IDAM IFAIL	EFAIL	T TOT DAT		DESCRIPTION		
			<del> </del>			·	
<b>0</b> 1	θ2	θ,	mmm		mmm	mmm	***************************************
		1	VIIIIIII		<i></i>		
DENSITY	SPH HEAT	TEMP1	TROOM	TMELT	1 v -	1 0	<del></del>
	1 000000	1	11100	1 1 1 1 1 1	V <sub>xy</sub>	Vyz	V <sub>ZX</sub>
E,	T E	· · · ·		T	Γ	***********	
	Ey	Ez	Gay	Gyz	Gzx	VIIIIIII	
Y.VICI D	I v viero	7 000		T 100 100 5	T =		
X-YIELD	Y-YIELD	Z-YIELD	XY-YIELD	YZ-YIELD	ZX-YIELD		
K1	K2	К3	1	CL	CQ.	PMIN	СН
	V-7-7	<u> </u>					
D1	D2	D3	D4	D5	SPALL	EFMIN	X1

Figure 2. Material Input Data

1 NNOD	E X1	J Y1	Z1	XN	YN	ZN	EXPAND
ROD NODE ID	ENTIFICATION C	ARD (15)					K, N, 12
	ШИШИ		THI THE	mmmm	mmmn	minimi	anninininininininininininininininininin
				<i></i>			
ROD NODE DE	SCRIPTION CAL	RD (415, 3F10.0)					
NOR NIR	NPLN IRAD	ZTOP	ZBOT	EXPAND	IIIIIIII		
OD NODE RA	DII CARD FOR IF	AD=0 (4F10.0)					
ROTOP	RITOP	ROBOT	RIBOT	HIIIIIII	THI THINK	THINITINI	THINING THE
OD NODE TO	P RADII CARD(S)	FOR IRAD-1	8F10.0)				
RT(NIR)		<u> </u>			I	RT(NOR)	
	TTOM RADII CAF	ID(S) FOR IRAD	►1 (8F10.0)	<b>~</b>	γ		
RB(NIR)	<u> </u>	L	<del></del>	ــــــــــــــــــــــــــــــــــــــ		RB(NOR)	<del></del>
00 H00E TO	D 0110E40E 040	0.500.000.4	ME10 M				
	P SURFACE CAR	D FOR HAD-1	(87 10.0)	<del></del>		770000	т — — — — — — — — — — — — — — — — — — —
ZT(NIR)	<b></b>			<u> </u>	<del></del>	ZT(NOR)	<del></del>
OD NODE BO	TTOM SURFACE	CARD FOR IRA	VD=1 (8F10.0)				
ZB(NIR)			1	T	<del>,</del>	ZB(NOR)	T
		L.—.	NOTE: IF N	R-0 BEGIN RAD	AND SURFAC	E CARDS WITH I	RT(1) AND RB(1)
OSE NODE ID	ENTIFICATION O	ARD (15)					
3 //////	<i>IIIIIIIIIII</i>	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	<i>IIIIIIIIIII</i>	<i>umumi</i>	IIIIIIIII	unnunni	
	ESCRIPTION CA						
NOR NIR	INOSE IRAD	ROTOP	RITOP	ZTOP	ZMIN		MINIMUR.
		4					
	OP RADII CARD(S	) FOR INAL = 1	(88-10.0)	<del></del>		T OT SHOOT	
RT(NIFI)	Ll		L	L	l	RT(NOR)	<del></del>
	ANI CARIOVSI EOE	2 IRAD = 1 /8F1/	0.0%				
nse Mone 71		10000 - 1700 1	<del></del>			7 740,000	
	ł ,		1	i .		I ZMANKUM)	
OSE NODE ZI ZM(NIR)	L		L	<u> </u>	L	ZM(NOR)	نـــــــــــــــــــــــــــــــــــــ
	<u> </u>		NOTE: IF NI	R = 0 BEGIN TOF	PADII AND ZW		RT(1) AND 2M(1)
ZM(NIR)	DE IDENTIFICAT	TON CARD (215		R = 0 BEGIN TOF	PRADII AND ZW		RT(1) AND 2M(1)
ZM(NIR)	DE IDENTIFICAT	TON CARD (215)				IN CARDS WITH	RT(1) AND ZM(1)
ZM(NIR)  AT PLATE NO	DOE IDENTIFICAT	TON CARID (215)				IN CARDS WITH	RT(1) AND ZM(1)
ZM(NIR)  AT PLATE NO  4 TYPE	DOE IDENTIFICAT					IN CARDS WITH	
ZM(NIR)  AT PLATE NO 4 TYPE  AT PLATE NO		N CARD FOR T				IN CARDS WITH	
ZM(NIR)  AT PLATE NO 4 TYPE  AT PLATE NO	DOE DESCRIPTION	N CARD FOR T	YPE = 1 (815, 5F	10.0)		IN CARDS WITH	
AT PLATE NO 4 TYPE AT PLATE NO NX NY	DOE DESCRIPTION	N CARD FOR T	YPE = 1 (885, 5F) X-EXPAND	10.0) X-PART		IN CARDS WITH	
AT PLATE NO 4 TYPE AT PLATE NO NX NY AT PLATE NO	DOE DESCRIPTION NZ NXEND	N CARD FOR T	YPE = 1 (885, 5F) X-EXPAND	10.0) X-PART		IN CARDS WITH	
AT PLATE NO 4 TYPE AT PLATE NO NX NY AT PLATE NO	DOE DESCRIPTION NZ NXEND	N CARD FOR T	YPE = 1 (86, 5F) X-EXPAND YPE = 2 (85, 5F)	10.0) X-PART	Y-EXPAND	IN CARDS WITH	Ž-EXPAND
LAT PLATE NO 4 TYPE LAT PLATE NO NX NY LAT PLATE NO NX NY	DOE DESCRIPTION NZ NXEND	N CARD FOR T	YPE = 1 (86, 5F) X-EXPAND YPE = 2 (85, 5F)	10.0) X-PART	Y-EXPAND	IN CARDS WITH	Ž-EXPAND

Figure 3a. Node Input Data

SPHEH	F MODE	: IDENTI	TTTTT	W CARD (15)	mm	m	mmm.	mmm	mm	mmmn
	11111	<i></i>	<i>m</i>		<i></i>	711111		<i></i>		<i></i>
SPHER	E NODE	DESCR	IPTION	CARD (215, 5X, 1	5, 3F10.0)					
NOR	NIR	IIII	IRAD	RO	RI		ZCG	HIIIII		ШИШИ
		RADII C	ARD(S)	FOR IRAD = 1 (8	F10.0)			·		
R(I	NIR)	<u></u>		<u> </u>				R(NOR)		
6 NABOR	FILLED	PLATE	NODE D	ESCRIPTION CA	ARD (715, :	5X, 3F10	.0)			
NNX	NNY	NNZ	MATL	NXENDNYEND	N		X-EXPAND	Y-EXPAND	DO	IIIIIIII
NABOR	FILLED	PLATE	SIZE CA	ARD (5E10.0)						
	(1		1	ZTOP	/XN		YN	HIIIII	THININI T	THI THINK
NAROR	BRICK	NODE ID	ENTIFIC	CATION CARD (I	5)					
7	IIIIX	IIIII	IIII		IIIII	IIIII	ullillilli	illillilli.	illillillilli	HIIIIIII
NAROO	BRICK	NODE O	FSCRIP	TION CARD (215	7 F10 0\				*****	<del></del>
MATL	IY		O	X1	7, 7 10.07 Y1		Z1	XN	T YN	T ZN
	<u></u>			<del></del>						

Figure 3b. Node Input Data

	NCOM	MATL	N1	N2	N3	N4	N5	N6	N7	N8	INC	IIIII	Ш	IIII	IIIII
		IDENTIF													
2															
ROD EI	LEMENT	DESCRI	PTION (	CARD (5	545)										
NOER	NIER	NLAY	N1	MATL	IIII							ШШ			
900 FI	EMENT	MATERI	AL CAR	n EOR I	AATI - (	1 (16)51									
MINER		marene	AL COURT		1	1		Γ	Τ	Τ	<u> </u>	M(NOER)			Т
MOSE E	LEMEN	T IDENTI	FICATIO	W CAR	D (15)										
3	IIII	IIIII	IIII	IIII	illilli	IIIII	IIII	IIII	IIIII	IIIII	IIII		IIII	IIII	THIII.
		T DESCR		MATL			m	m	m	m	m		m	m	m
HOLI	INCI			MATIL		<i></i>	<i></i>	<i></i>	<i></i>	,,,,,,,	777777	<i></i>	<i></i>	<i></i>	<i></i>
		MATER	IAL CAP	D FOR	MATL -	0 (1615)			<del></del>						·
M(NIER	1 1	i I			l		1	l .		1		MANOEMI			1
	LATE EU	EMENT I	DENTIF	ICATIO	N CARD	(215)	<u> </u>	1	<u> </u>	<u> </u>	<u> </u>	M(NOER)	<del></del>		<b></b>
FLAT PI	TYPE					(215)						MINOEN)			
FLAT PI	ATE DE	EMENT I		RD (585)											
FLAT PI	ATE DE	SCRIPTI	ON CAF	RD (585)								<del></del>			
4 FLAT PI	ATE DE	SCRIPTI NLZ	ON CAF	RD (515) MATL											
FLAT PI 4 FLAT PI NLX	ATE DE NLY	SCRIPTI NLZ	ON CAF	RD (515) MATL	VRO (15)										
FLAT PI 4 FLAT PI NLX	ATE DE NLY	SCRIPTI NLZ	ON CAF	RD (515) MATL	VRO (15)										
FLAT PI 4 FLAT PI NLX SPHERIE	ATE DE NLY	SCRIPTI NLZ	ON CAF	RD (5IS) MATL TION CAR	VRD (15)	5X, 2(5)									
FLAT PI 4 FLAT PI NLX SPHERE 5	ATE DE NLY E ELEME	SCRIPTI NLZ	ON CAF	RD (5IS) MATL TION CAR	VRD (15)	5X, 2(5)									
FLAT PI 4 FLAT PI NLX SPHERE 5 SPHERE NOER	ATE DE NLY  E ELEME ELEME NIER	SCRIPTI NLZ ENT IDEN	ON CAF	RD (515) MATL TION CAR ON CAR MATL	ARD (15)	5X, 2IS)									
FLAT PI 4 FLAT PI NLX SPHERE 5 SPHERE NOER	ATE DE NLY  E ELEME ELEME NIER	SCRIPTI NLZ ENT IDEN	ON CAF	RD (515) MATL TION CAR ON CAR MATL	ARD (15)	5X, 2IS)									
FLAT PI 4 FLAT PI NLX SPHERE 5 SPHERE NOER	ATE DE NLY  E ELEME ELEME NIER	SCRIPTI NLZ ENT IDEN	ON CAF	RD (515) MATL TION CAR ON CAR MATL	ARD (15)	5X, 2IS)									
FLAT PI  FLAT PI  NLX  SPHERE  SPHERE  SPHERE  SPHERE  SPHERE	ATE DE NLY  E ELEME ELEME NIER	SCRIPTI NLZ ENT IDEN	ON CAF	RD (515) MATL TION CAR ON CAR MATL	ARD (15)	5X, 2IS)									
FLAT PI 4 FLAT PI NLX 5 SPHERE NOER SPHERE RINIER	ATE DE NLY E ELEME NIER ELEME FILLED F	SCRIPTI INLZ INT IDEN	ON CAF N1 ITIFICAT CRIPTIC N1 ERIAL C	RD (5IS) MATL TION CAR MATL ARD FO	O (215, 1)	5X, 2IS) -= 0 (16	(is)					M(NOER)			
FLAT PI  FLAT PI  NLX  SPHERE  SPHERE  NOER  SPHERE  KINIER	ATE DE NLY E ELEME NIER ELEME FILLED F	SCRIPTI INLZ INT IDEN	ON CAF N1 ITIFICAT CRIPTIC N1 ERIAL C	RD (5IS) MATL TION CAR MATL ARD FO	O (215, 1)	5X, 2IS) -= 0 (16	(is)								
4 LAT PI NLX 5 PHERE NOER PHERE (NIER ABOR 6	ATE DE NLY E ELEME NIER FILLED F	SCRIPTI INLZ INT IDEN	ON CAF N1 ITIFICAT CRIPTIC N1 ERIAL C	RD (5IS) MATL TION CAR MATL ARD FO	O (215, 1)	5X, 2IS)  ON CARR	(is)					M(NOER)			

Figure 4. Element Input Data

		04BB /	4.001												
		CARD (													
	× 111 110		-									<del></del>			
IDENT	FICATIO	ON CARE	) (515, 5X	5F10.0	)										
CASE	CYCLE	<b>IPRES</b>	CHANG	IHRG	11111	VFF	ACT	PM	AX .	VNR	EF	AF	MAX	ASE	RR
	RATION RAX	TIME IN	CREMEN	T CARL		<u> </u>	4AX	CP	4AX	FV	MX	m	m	IIIII	viiiii
	-	1 011		3,	<u></u>	<u> </u>		1 0, .	-			77777	<i>iiiiii</i>	<i></i>	777777
PRESS	URE CA	ARDS FO	R IPRES	= 2 - AS	S REQUI	RED (61	5, F10.0)								
ELE1	ELEN	ELEIN	N1	NN	NODIN	C PI	RES	IIIII		IIIII		ШШ			
				•											
DI ANI	K CARE		BIC! I	חבח מו	NLY FOF	10000	_ 2								
BUNN	N WANL	<u> </u>	WOLU	DED O	uci ror	1 IF NE.S									
TIME -	PRESSI	JRE CAF	NOS FOR												
PTIM	ME		P(T)	IIII	IIIII										
				-											
BLAN	K CARD	. 5	INCLU	DED OF	NLY FOR	IPRES	<b>-</b> 2								
			FOR CH		<del></del>		· .	1 DI OF	INCAH.	4440			m	m	emm
TDA	IOP	NODE	PNODE	ELE	PELE	NSLID	NPLOT	LPLOT	NFAIL	NAB	PNAB		111111	,,,,,,,	711117
DESK	SNATED	ELEME	NT FAILL	IRE CAI	RD - FOF	R NFAIL	> 0 (16년	5)							
EF1	EF2	T	T		Γ	Г	T	<u> </u>	EFN			T			
	<u> </u>		*			<u> </u>		·							
CHANG	E ADO	CARD FO	OR CHAN	G = 2 C	R 3 (F10	).0. 1115	)								
TA	DD	NSLID	XYZRIG	SPLIT	NIR	NNR	N1L	NOR	NIR	NPL	NRS	IPRINT	IIII	IIIII	
				•	<del></del>	•		·							
TARGE	T SCAL	E / SHIFT	r/ROTA	E CARI	FORC	HANG =	2 OR 3	(7F10.0)							
	CALE		ALE	ZSC		XSH		ZSH		ROTA	ATE	SLA	NT	IIIII	
			ODE DA						י ט:						
<u> </u>	K CARD						NG = 20								
			LEMENT	_					JIRED						
BLAN	K CARD		ENDS	ELEMEI	NT DATA	FORC	HANG =	2 OH 3							
						_									
NSLID [	DATA - A	NS REQU	JIRED FO	R CHAI	VG = 20	H3)	SAM" F	ORMAT	AS USE	D IN PR	EPROC	ESSOR			
NHST	DATA - A	S REQU	WRIED FO	R CHAN	G = 2 O	43 <i>J</i>									
TARGE	T VELO	CITY CA	RID FOR	CHANG	= 2 OF 3	30X. 3	F10.0)								
			TITIL.			TXE		TYD	от	TZD	or	IIII	IIIII	illi.	
															لنبينا

Figure 5a. Main Routine Input Data

	eve	15, 5X, 4F		LOLOT	$\overline{vm}$	DT SYS	TSYS	DT NODE	TNODE	
CTCL	: 1 313	Iconu	NFLOT			DI 313	1 .0.0		1	VIIIIIII
DESIG	NATED	NODES (	APRS.	AS REO	WIRED (1	AIS)				
	·	T	JANUS .	AS REG	OH ICD (1	<del></del>	<del></del>	<del>1 1</del>	I NN	<del></del>
N1	N2	1	<u> </u>				<u> </u>		THE	
DESIG	NATED	ELEMEN	TS CAR	S-ASI	REQUIRE	D (1615)				
DECK	NATER	C: CLACL	TC CAD	SC 4C1	DE() NOC	D /1865				
	NATED E2	ELEMEN	TS CAR	)S - AS I	REQUIRE	D (1615)	т т	<del>1 1</del>	EN	<del>1   1   1   1   1   1   1   1   1   1  </del>
DESIG E1	<del></del>	ELEMEN	TS CAR	OS - AS I	REQUIRE	D (1615)			EN	
E1	E2	I			I				EN	
E1	E2	CARDS	- AS REG	QUIRED	(2F10.0, 3	345)			EN EN	

Figure 5b. Main Routine Input Data

GEOMETRY PL		10.0, 212, 4X, 212	, 18X, A30)				<del></del>
1 CYCLE	TIME					TITLE	
	AXIS VIEW	1	LMATL FAIL				
		= 2 (6F10.0, 2I5) YMAX	- Valai	ZMAX	ZMIN	LMAX LMI	VIIIIIIIIV
XMAX	XMIN	TMAX	YMIN	ZMAX		CHICA CHIL	<u>- 1111111111</u>
30 PERSPECTIV	VE CARD FOR V	/IEW = 4 OR 8 (6)	F10.0. I5)				
XEYE	YEYE	ZEYE	XPLANE	YPLANE	ZPLANE	LHIDE	
				•			
		D (215, F10.0, 212	, 2X, 212, 10X, F1				<del></del>
2 CYCLE	TIME			VSCALE		TITLE	
	AXES VIEW		ARROW EDGE				
PLOT LIMITS CA	ARD FOR AXES	= 2 (6F10.0)					
XMAX	XMIN	YMAX	YMIN	ZMAX	ZMIN		
3D PERSPECTIVE	YEYE	/IEW = 4 (6F10.0,	) XPLANE	YPLANE T	ZPLANE	THININ T	
AETE	72,0	LEIC	A DAVE	1.04.2		AIIIIIII	<i></i>
CONTOUR PLOT	T CARD (215, F1	0.0, 212, 2X, 412,	16X, A30)				
TYPE CYCLE	TME					TITLE	
	AXES	1   1	LPRINT				
	VIEW	_	SYMBOL				
	EDGE		NLINE				
PLOT LIMITS CA				<del> </del>	ZMIN	IIIIIII	emminimi
XMAX	XMIN	YMAX	YMIN	ZMAX	ZMIN	Allillilli	<i></i>
CONTOUR SPE	CIFICATION CA	BD (8F10.0)					
VAR (1)	VAR (2)	1 (0. 10.0)	1	T T		VAR(NLINE)	
	· · · · · · · · · · · · · · · · · · ·	<del></del>	<u> </u>	<u> </u>			
IYPE	YARK	BLE PLOTTED					
3		SURE					
4		MISES STRESS VALENT PLASTK	CTDAN				
5 6	DAMA		Johnson				
7		ERATURE					
8	PLAS	TIC WORK PER I	NITIAL VOLUME				
9	INTER	MAL ENERGY P	ER INITIAL VOLU	ME			
10	LOG (	10) STRAIN RAT	E				
10	LOG (	10) STRAIN RAT	E				
BLANK CARE		(10) STRAIN RAT		ONTOUR PLOTS			
BLANK CARE	DI 3 ENDS		ELOCITY AND CO	ONTOUR PLOTS			
BLANK CARE	ENDS	GEOMETRY, VE	ELOCITY AND CO	ONTOUR PLOTS		TITLE	
BLANK CARE	DI 3 ENDS	GEOMETRY, VE	ELOCITY AND CO	ONTOUR PLOTS		TITLE	
BLANK CARE	DI 3 ENDS	GEOMETRY, VE	ELOCITY AND CA	ONTOUR PLOTS		TITLE	
BLANK CARE	DI 3 ENDS DS PLOT CARD TIME	(215, F10.0, 412, 2	ELOCITY AND CA			TITLE	
BLANK CARI INTERNAL LOAI 15 CYCLE	DI 3 ENDS DS PLOT CARD TIME	(215, F10.0, 412, 2	ELOCITY AND CA		BMIN	TITLE	
BLANK CARE INTERNAL LOAE 15 CYCLE	OS PLOT CARD TIME	26, F10.0, 412, 215, F10.0, 412, 412, 412, 412, 412, 412, 412, 412	ELOCITY AND CO 22X, A30)	XES, IP, IV, IM	BMIN		

Figure 6. Postprocessor Input Data for State Plots

SYSTEM	PLOT CARDS - AS REQUIRED (215, 5X,	F5.0. 4F10.0. A	201			
	AXES THAX	TMIN	VMAX	VMIN	TITLE	
	LOADS PLOT CARDS - AS REQUIRED  AXES LAYER SCALE   TMAX	(315, F5.0, 4F1)	0.0, A20) VMAX	T VMIN T	TITLE	
	MES PATER BOALE   IMAX	IMM	VINOCK	1 AMBA 1	HILE	
INDIVIDU	L NODE PLOT CARDS - AS REQUIRED	(315, F5.0, 4F1	0.0, <b>A20</b> )			
	AXES NODE SCALE TMAX	TMIN	VMAX	VMIN	TITLE	
	LELEMENT PLOT CARDS - AS REQUI	RED (315, F5.0,	4F10.0, A20)	T VMIN T	TITLE	
			1 1			
BLANK C						
BOWN C	ARD S					*
TYPE	YARIABLE PLOTTED					
1-4	ENERGIES: TOTAL (1), KINETIC (2),	INTERNAL (3), I	PLASTIC WORK	(4)		
5 - 7	XYZ MAXIMUM COORDINATES	, ,				
8 - 10	XYZ MINIMUM COORDINATES					
11 - 13	XYZ CENTERS OF GRAVITY					
14 - 16	XYZ LINEAR MOMENTA			}	SYSTEM DATA	
17 - 20	XYZ VELOCITIES (17 - 19) AND NET	VELOCITY (20)				
21 - 23	XYZ ANGULAR MOMENTA	,				
24 - 26	XYZ ANGULAR VELOCITIES					
27 - 29	INTERNAL LOADS: AXIAL (27), SHE	EAR (28), BEND	ING (29)	1	INTERNAL	
30 - 32	XYZ NODE POSITIONS			-	LOADS DATA	
33 - 35	XYZ NODE VELOCITIES			į		
36 - 38	XYZ NODE ACCELERATIONS			}	INDIVIDUAL NODE DATA	
39	NODAL PRESSURES					
40	ELEMENT PRESSURES			1		
41 - 43	XYZ NORMAL STRESSES					
44 - 46	SHEAR STRESSES: X-Y (44), X-Z (45	D. Y-Z (48)				
47	VON MISES STRESS	,, · - ( · - ,				
48	EQUIVALENT PLASTIC STRAIN			}	INDIVIDUAL ELEMENT DATA	
49	TEMPERATURE					
50	INTERNAL ENERGY PER INITIAL VOL	UME				
51	PLASTIC WORK PER INITIAL VOLUME					
52	DAMAGE	-				
	RATIO: MEAN STRESS / VON MISES	CTDECC				
53	TATIO. MEAN STRESS / YUN MISES	317E33		)		

Figure 7. Postprocessor Input Data for Time Plots

MARIAGE.	EXPANO																	
<b>OF</b>		.7		.0		.9		.0	,	.1	1	.2	1	, 3	1	,4	1.5	
INCRE- MENTS	<u>4,</u>	<u> </u>	3.	<u>1</u>	<u>\$.</u>	<u>A.</u>	3, 3	3-4	4: 4	<u>A.,</u>	<u>Δι</u> <u>Δ</u>	<u>4</u>	<u>4,</u>	<u>4</u>	Δ; 3	<u>A-</u>	<u>3,</u>	<u>a</u>
2	1,176	.824	1,111	. 500	1.053	.947	1.0	1.0	.952	1.046	. 909	1.001	. 870	1.130	. 823	1.167	. 200	1.200
3	1,370	.671	1.230	.787	1,107	. 807		1	. 906	1.097	. 824	1,167	.752	1.271	. 640	1,340	.632	1,421
4	1.579	.542	1,355	.604	1.163	. 840			. 862	1,147	. 745	1,286	.647	1.420	.563	1.545	.402	1.662
\$	1.803	.433	1,407	.600	1,221	. 80 1			.319	1,199	. 672	1,393	. 553	1.579	. 457	1,755	.379	1.919
6	2.040	س.	1.626	. 533	1,261	. 756			, 778	1.252	. 604	1.504	. 470	1.746	. 366	1,977	.289	2.192
,	2,286	.260	1,772	.464	1,342	.713			. 738	1.307	. 542	1,618	. 390	1.922	. 293	2.210	.218	2,467
•	2,547	.210	1.923	.403	1.405	.672			. 700	1.367	.465	1.737	. 135	2,104	. 233	2.452	. 162	2.775
•	2.814	, 162	2.679	.340	1,460	.632			.663	1,421	.43	1.861	. 201	2, 293	.183	2.702	. 120	3.080
10	3.007	. 125	2.241	. 301	1.535	. 595			.627	1,479	. 345	1,988	. 235	2.466	.143	2.959	.086	3, 392
12	3.651	.072	2,577	.221	1,672	, 525			. 561	1.601	. 303	2.253	. 161	2.093	.006	3,460	.047	4.031
14,	4,229	.041	2.929	.161	1,815	.461			. 500	1.726	.237	2.530	.109	3,315	.051	4.036	.024	4,662
16	4.816	.023	3,293	,116	1.964	.404			. 445	1.450	, 183	2.819	.073	3,740	.030	4.592	.012	5.341
10	5,409	.013	3.666	.083	2.118	. 153			. 795	1,995	. 140	3,117	.046	4, 191	.017	5.   55	.006	6.004
20	6.003	.005	4.037	.046	2.246	.273	] }		.349	2.102	.089	3.407	.024	4.634	.007	5,719	.002	6.660

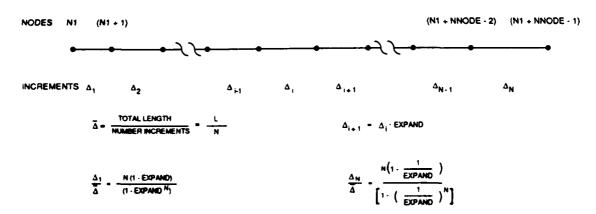


Figure 8. Nodal Spacing for Various Expansion Factors

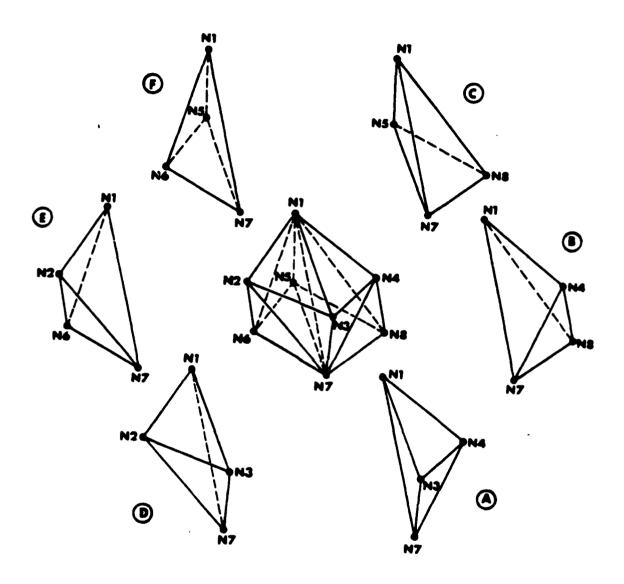


Figure 9. Arrangement of Six Tetrahedra into a Composite Brick Element

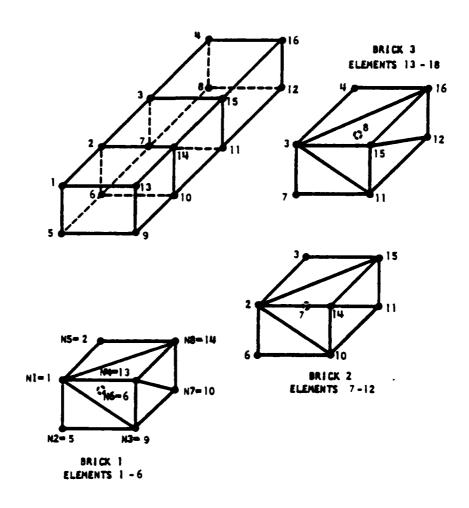


Figure 10. Node/Element Input Data Example

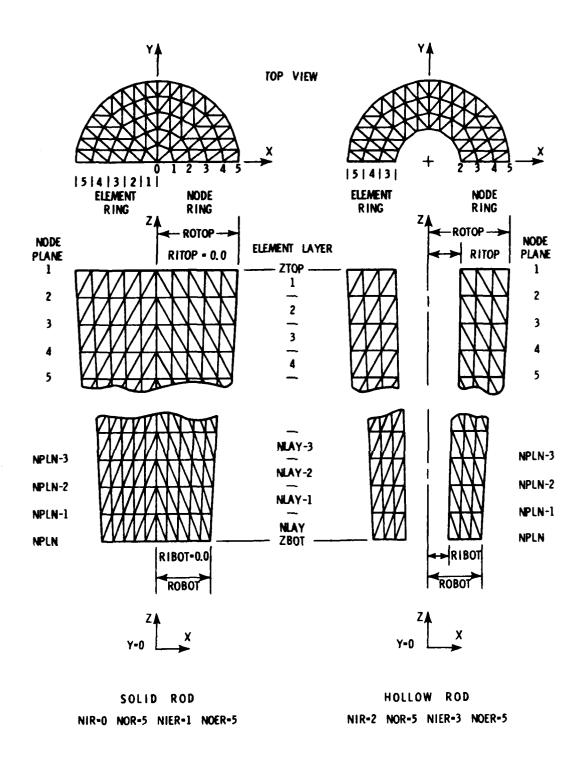


Figure 11. Rod Shape Geometry

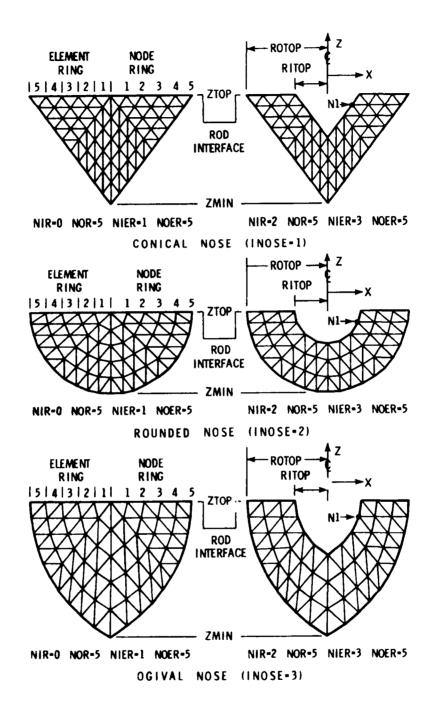
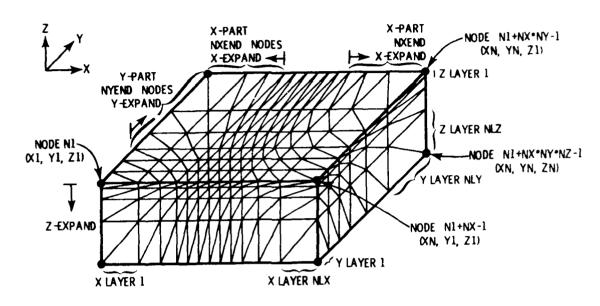
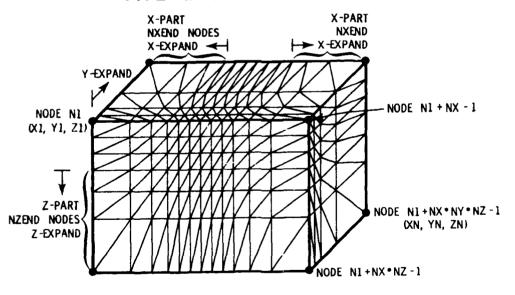


Figure 12. Nose Shape Geometry

TYPE - 1 (HORIZONTAL LAYERS)



TYPE - 2 (VERTICAL LAYERS)



AND THE PROPERTY OF THE PARTY O

1555 COSC

Figure 13. Flat Plate Geometry

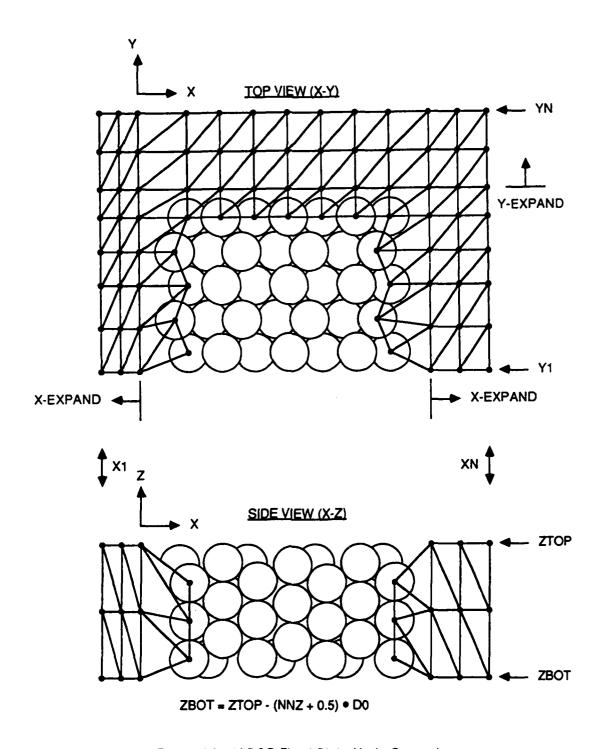


Figure 14. NABOR Filled Plate Node Geometry

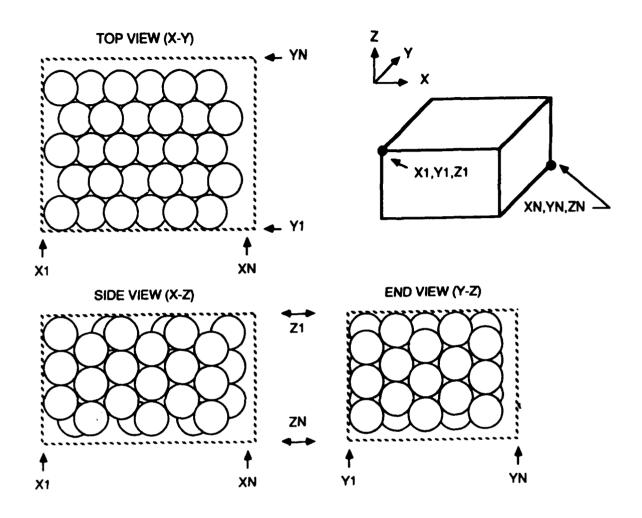


Figure 15. NABOR Node Geometry

NUMBER	RO	D •	NO	SE •	SPI	IERE •	
OF RINGS	NODES PER PLANE	ELEMENTS PER LAYER	NODES **	ELEMENTS	NODES	ELEMENTS	
0	1	-	0	<u>-</u>	1	-	
1	6	12	6	12	18	24	
2	15	48	30	96	75	192	
3	28	108	84	324	196	648	
4	45	192	180	768	405	1536	
5	66	300	330	1500	726	3000	
6	91	432	546	2592	1183	5184	
7	120	588	840	4116	1800	8232	
8	153	768	1224	6144	2601	12288	
9	190	972	1710	8748	3610	17496	
10	231	1200	2310	12000	4851	24000	
11	276	1452	3036	15972	6348	31944	
12	325	1728	3900	20736	8125	41472	
13	378	2028	4914	26364	10206	52728	
14	435	2352	6090	32928	12615	65856	
15	496	2700	7440	40500	15376	81000	
16	561	3072	8976	49152	18513	98304	

<sup>.</sup> ONLY HALF GENERATED

Figure 16. Summary of Nodes and Elements in Various Shapes

<sup>\*\*</sup> DOES NOT INCLUDE NODES AT ROD INTERFACE

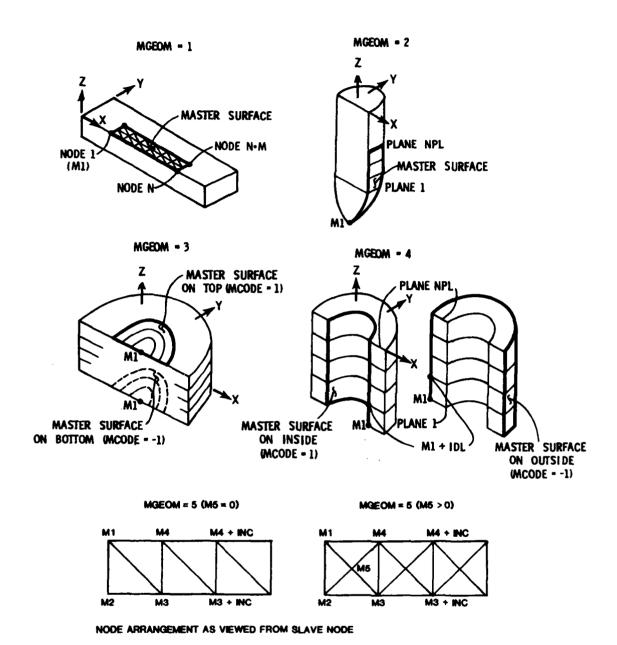


Figure 17. Master Surface Options for Sliding Interfaces

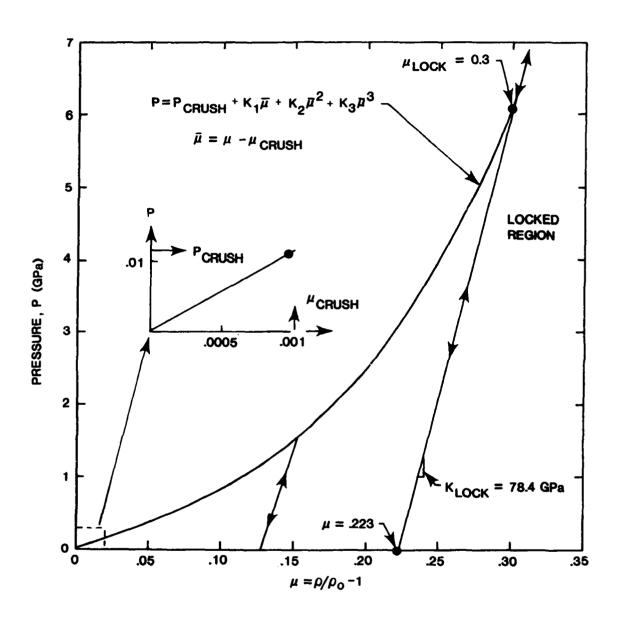


Figure 18. Pressure Model for Crushable Solids. Specific Data Shown are for Concrete

Transport | Transport

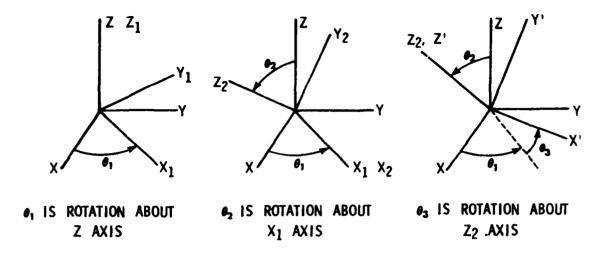


Figure 19. Euler Angles for Principal Material Axes X¹, Y¹, Z¹ Relative to Initial System Axes X, Y, Z

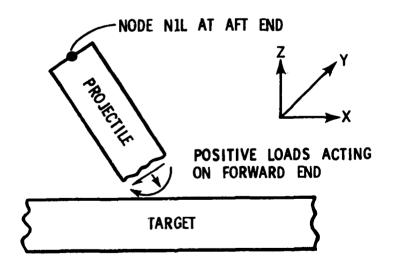


Figure 20. Sign Convention for Internal Loads

#### 1. INPUT DATA FOR THE PREPROCESSOR

The functions of the Preprocessor are to define the initial geometry and velocity conditions, and to determine the memory size requirements for the Main Routine. The descriptions which follow are for the data in Figure 1. Consistent units must be used, and the unit of time must be seconds.

It is possible to interject user comments into the data by use of a \$ character. If the \$ is in the first column of the card, that entire card is ignored as input data. If the \$ is beyond the first column in the card, then the \$ and all data to the right of the \$ are ignored.

**Description Card (A80)** – A description of the problem provided by the user.

#### Miscellaneous Card (14I5) -

CASE

= Case number for run identification.

PRINT

0 will not print individual data for each node and element.

1 will print individual node and element data, and complete sliding interface data.

2 will print node data for nodes with y = 0 and element data for elements with one face on the y = 0 plane.

SAVE

0 will not write results on restart file.

1 will write on restart file.

**NSLID** 

Number of sliding surfaces.

100 gives a rigid frictionless surface on the positive side of the plane described by  $\mathbf{x} = 0$ . If the equations of motion cause a node to have a negative  $\mathbf{x}$  coordinate, then the  $\mathbf{x}$  coordinate is set to zero and the  $\mathbf{x}$  velocity is also set to zero. NABOR nodes with an  $\mathbf{x}$  coordinate less than one radius have the  $\mathbf{x}$  coordinate set to one radius and the  $\mathbf{x}$  velocity set to zero.

**XYZRIG** 

10 gives a rigid frictionless surface at y = 0.

1 gives a rigid frictionless surface at z = 0.

0 or blank will ignore this option.

These options can be combined by addition. For example, 111 gives rigid frictionless surfaces on all three major planes.

O will perform the sliding surface computations after the updated velocities and displacements are determined from the usual equations of motion. Contact is established as long as the slave node interferes with the master surface before the velocities and displacements are adjusted in the sliding surface routines. This option is the most reliable and should be used for complicated sliding surfaces, which include double pass and intersecting sliding surfaces. It must be used for the eroding interface option. For relatively low velocity impact problems, where there is limited deformation, this option can introduce significant errors in the form of excessive deformation and internal energy. A double pass sliding surface is a pair of sliding surfaces that have the role of Master and Slave interchanged. The two sliding surface passes, one from each sliding surface, prevent either surface from penetrating the other.

SPLIT

1 will perform the sliding surface computations after the updated velocities are determined but before the updated displacements are determined. This should be used if the sliding surfaces do not require a double pass or the eroding interface option. Contact is first established when the slave node interferes with the master surface. Thereafter, a slave node is considered to be in contact until the preadjusted normal velocities between the two surfaces are separating rather than closing. This approach minimizes the distance the slave node is moved to place it on the master surface and is therefore more accurate. If there are no sliding surfaces, either option can be used (SPLIT = 0 or SPLIT = 1).

N<sub>1</sub>R

The first node in a series of consecutive nodes, which act as a rigid body. This option automatically restrains the nodes in the y direction and leaves them free to move in the x and z directions. The rigid body nodes cannot be restrained in either the x or z directions and they cannot be designated as slave nodes on sliding surfaces.

**NNR** 

= The last rigid body node. All notes from N1R to NNR are treated as a rigid body. This node number can control the required bandwidth since the minimum number of nodes in memory must be at least equal to NNR.

N<sub>1</sub>L

= The node number of the innermost node at the top free end of a cylindrical projectile. This is used if it is desired to compute internal loads in a slender projectile. If this option is used, the nodal geometry must be consistent with the arrangement of nodes generated by the rod node generator described later. Leave blank if not used.

NOR

= The outer ring number of the rod if internal loads are requested.

NIR

= The inner ring number of the rod.

NPL

= The number of planes of nodes in the rod for the internal loads.

0 indicates the constants in the material library have English

units (pound/inch/second/degree Fahrenheit).

UNIT

1 indicates the constants in the material library are converted to

Standard International (SI) units.

**NRST** 

= Number of groups of nodes to have restraints redefined.

Material Data Cards — Material data can be defined by the user or taken from the material data library. Specific instructions are presented later. End material data with a blank card.

# Projectile Scale/Shift/Rotate Card (7F10.0) -

XSCALE

= Factor by which the x coordinates of all projectile nodes are multiplied. Applied after the coordinate shifts (XSHIFT, ZSHIFT) described later. Must use XSCALE = YSCALE = ZSCALE = 1.0 if any NABOR nodes are used.

**YSCALE** 

= Factor by which the y coordinates are multiplied.

**ZSCALE** 

= Factor by which the z coordinates are multiplied.

**XSHIFT** 

Increment added to the x coordinates of all projectile nodes (length). Applied before the scale factors (XSCALE, YSCALE, ZSCALE).

**ZSHIFT** 

= Increment added to the z coordinates (length).

ROTATE

Rotation about the y axis (at x = z = 0) of all projectile nodes (degrees). Applied after the coordinate shifts (XSHIFT, ZSHIFT) and the scale factors (XSCALE, YSCALE, ZSCALE). Clockwise, as viewed from a negative y location, is a positive rotation.

**SLANT** 

= The angle (degrees) used to redefine the x coordinates of all projectile nodes with the relationship  $X_{new} = X_{old} + Z$  tan (SLANT). This takes vertical lines of nodes and aligns them at an angle, SLANT, with the vertical. Applied after the other SCALE/SHIFT/ROTATE operations.

Node Data Cards for Projectile — These cards are required to define the projectile nodes. If a node is at the interface of the projectile and the target and contains mass from both the projectile and the target, it must be included with the projectile nodes. The nodes will be numbered consecutively. Specific instructions for node input data are presented later. End projectile node data with a blank card. Include blank card even if there are no projectile nodes.

Target Scale/Shift/Rotate Card (7F10.0) — Same as Projectile Scale/Shift/Rotate Card except it applies to the target nodes. Must be included even if there are no target nodes.

Node Data Cards for Target — Similar to node data cards for projectile. Specific instructions are presented later. End target node data with a blank card. Include blank card even if there are no target nodes.

Element Data Cards for Projectile – These cards are required to define the projectile elements. The element numbers will be numbered consecutively. Specific instructions are presented later. End projectile element data with a blank card. Include blank card even if there are no projectile elements.

Element Data Cards for Target — Similar to element data cards for projectile. Specific instructions are presented later. End target element data with a blank card. Include blank card even if there are no target elements.

Sliding Surface Identification Card (1015, 3F10.0) — Each sliding surface contains one Identification Card, one or more Master Definition Cards and cards (if required) describing the slave nodes. If there is more than one sliding surface, all data for the first surface are input before beginning data for the second surface. The sliding surfaces should be input in order of the maximum node number on each sliding surface. The mass and spacing of the slave nodes should not be significantly greater than that of the master nodes in the initial or deformed geometry unless a double pass is used. Also, the slave nodes cannot be restrained in the z direction. The nodal bandwidth will be set to contain all sliding surface nodes for a specific sliding surface. The user should be familiar with the node generators before proceeding.

**MGEOM** 

A code describing the geometry of the master surface. Must be 1,
 2, 3, 4, 5, as shown in Figure 17. Specific geometries are described in the Master Definition Cards.

A code describing the search routines used to find the appropriate triangular plane on the master surface. Whenever possible use the specialized searches, SEEK =  $(\pm 1, \pm 2, \pm 3)$ . The specialized routines can be used whenever the master surface is a single valued function of two coordinates (i.e., any vertical line parallel to a specified axis must not pass through the master surface at more than one point). For eroding sliding surfaces set SEEK = 4.

- -1 For all slave nodes on the negative x side of the master surface.
  - 1 For all slave nodes on the positive x side of the master surface.
- -2 For all slave nodes in the negative y side of the master surface.
- 2 For all slave nodes on the positive y side of the master surface.
- -3 For all slave nodes on the negative z side of the master surface.
- 3 For all slave nodes on the positive z side of the master surface.
- 4 For the generalized search routine. Use of this option can require significant additional CPU time. Every master triangular surface is considered for each slave node. If a slave node is contained in the triangular projection (onto a principal plane) of one or more master surface triangles, and if it is close to the triangular plane  $|\delta_n|$  < REFVEL · DT, then the master plane closest to the slave node is selected.  $\delta$  n is the normal distance between the slave node and the master plane. REFVEL is the reference velocity given on this card and DT is the integration time increment. If the slave node projection is not within any master triangular projections but is close normally to at least one triangular plane  $|\delta_n|$  < REFVEL · DT, and if the disfrom the slave node projection to the master triangular projecttion is small,  $|\delta_{edge}|$  < REFVEL DT, then the master triangle with the smaller |8 edge | is selected. More detail is given in Reference 10.

IT

SEEK

Number of velocity iterations. Errors in the velocity match lead to errors in the deviator and shear stresses, but generally not the pressure. (For anisotropic materials, if the pressures are determined incrementally, then there can be errors introduced into the pressure.) For high velocity impact, where the pressures are much higher than the deviator and shear stresses, a relatively low value of IT = 1 or IT = 2 can be used. For lower pressure problems, higher values should be used, IT = 2 to IT = 5. The velocity iterations, and the corresponding searches on the master surface, are performed only for those slave nodes found to be in contact during the first iteration. For sliding surfaces with many slave nodes in contact and many master nodes, high values of IT

can lead to significant increases in CPU time. This is especially true if SEEK = 4. For the eroding interface option (ERODE > 0), use IT = 1.

M1

Node number of the first node on the master surface. These will be defined by the Master Definition Cards. The first node is used to define the master surface, but it may not be the lowest numbered master node.

S1

= The lowest numbered slave node. Leave blank for NSN = 0.

SN

= The highest numbered slave node. Leave blank for NSN = 0.

**NSN** 

= The total number of slave nodes in the sliding surface. If all nodes between S1 and SN are slave nodes (NSN = SN - S1 + 1), no additional input data are necessary. Otherwise, slave nodes are read individually or in groups. For NSN = 0, the number of slave nodes is calculated to be the number of nodes in the slave box whose dimensions are given on the Slave Node Limits Cards. In some instances groups of nodes are added to those defined by the slave box. Slave nodes cannot be restrained in the z direction.

NSG

Numbers of groups of slave nodes to be read. If NSG = 0, the nodes are either consecutive between S1 and SN, or they are read individually, or they are designated by region.

**ISR** 

= 1 will release slave nodes from the plane of symmetry when they interact with master surface. May use in conjunction with MGEOM = 2 for deep penetration problems. Option not used if left blank.

**NAB** 

= 1 when the slave nodes are NABOR nodes; leave blank when slave nodes are regular (not NABOR) nodes. Slave nodes, for a specific sliding surface, must be all of one type.

**FRICT** 

= The coefficient of sliding friction.

REFVEL

Reference velocity, which when multiplied by the integration time increment, gives a reference distance. Slave nodes are considered to be associated with a particular master plane only when they are within this reference distance. It is recommended that REFVEL be 1.0 to 1.5 times the relative impact velocity, or the detonation velocity of the explosive.

**ERODE** 

Equivalent plastic strain (or volumetric strain), which if exceeded by any element on the master surface, will cause the element to be completely failed. Subsequently, the master surface will be redefined to go around the failed element. This allows for penetration/perforation of thick plates. If ERODE = 0, then erosion is not used. The specific erosion algorithm is described in Reference 8. Because total failure of the elements must be achieved by the eroding interface algorithm, it is important that EFAIL (a material property) be much greater than ERODE.

### Master Definition Card for Plate Geometry (MGEOM = 1) (915) -

**NML** 

Number of nodes per row of master nodes. NML is equal to N in Figure 17. Each row of master nodes must have the same number of nodes.

**NMW** 

Number of rows of master nodes. NMW is equal to M in Figure 17. Note that a properly described master surface will pass the following test. Place a right-handed triad of orthogonal vectors on node M1. Point the first vector (thumb) away from the master surface towards the slave nodes. Point the second vector (index finger) down the row of nodes starting at M1. The third vector (second finger) will then point in the direction of the remaining rows of nodes. Two of the corner nodes will pass this test when defined as M1 and the other two corner nodes will fail the test.

IDL

The node number increment along the rows of master nodes. If M1 = 100, NML = 6, and IDL = 2, then the first row of nodes in the master surface consists of nodes 100, 102, 104, 106, 108, 110. IDL may be negative.

**IDW** 

= The node number increment between the first node of each row. If IDW = 20 and M1, NML and IDL are as described in the preceding description of IDL, then the second row of master nodes consists of nodes 120, 122, 124, 126, 128, 130. IDW may be negative.

1 is for the diagonal orientation shown in Figure 17.

IDIA

2 is for the other diagonal orientation where the diagonals go in the general direction from the first master node to the last master node

**NBOT** 

Lowest numbered node on the bottom surface. Used only for an eroding plate to detect erosion through the bottom of the plate.
 All plate nodes equal to or larger than NBOT are considered to be on the bottom of the plate.

NLAST

The largest node number which will be on any element on the surface of an eroding sliding surface. Required only for an eroding interface. The largest node number on the plate is adequate but a more precise number can reduce the bandwidth required for the sliding surface. A small estimate of NLAST will result in a small estimate of the required bandwidth, but the bandwidth is checked dynamically during erosion and the problem will stop if not enough memory is available for the bandwidth actually required.

**MGNXT** 

MGEOM for the next geometry describing part of the master surface. Leave blank when the master surface description is complete.

M1NXT

M1 to be used with the next geometry specified by MGNXT. Leave blank when MGNXT is blank.

Master Definition Card for Nose-Rod Geometry (MGEOM = 2) (315, 20X, 215) — This option can be used for deep penetration problems when the projectile is significantly harder than the target. The master surface contains all external triangular planes on the nose and specified triangles in the rod. The nose and rod geometry must be consistent with the grid generators in Figure 11 and 12. The first master node, M1, is at the tip of the nose as shown in Figure 17.

For this option the slave nodes are generally in the target. It is recommended that ISR = 1 in the Sliding Surface Identification Card, if there are any restrained nodes on the plane of symmetry at y = 0. Use of this option will release the restraint when the slave node comes in contact with the master surface.

NOR

= Outer node ring number of the nose and the rod of the projectile.

NIR

Inner ring number.

NPL

= Number of planes of nodes in the rod included in the master surface. The interface of the rod and the nose is considered to be plane number 1. If NPL = 2, then the master surface would include all the triangular faces on the nose, plus those between the interface plane of nodes and the plane of nodes directly above the interface plane.

MGNXT, M1NXT  Data for additional master surfaces, described previously for MGEOM = 1.

Master Definition Card for Disk Geometry (MGEOM = 3) (215, 15X, 415) — This option can be used if the master surface is on a disk whose nodal arrangement is equivalent to that of the rod generator. (A disk is simply a very short rod or cylinder.) The first node, M1, is at the center of the master surface as shown in Figure 17.

**NRING** 

A LEGISTICAL TODOS DO DESCRIPTION SERVICE SONO DE LA CONTRACTION DEL CONTRACTION DE LA CONTRACTION DE

= Maximum node ring number included in the master surface.

1 indicates the master surface is on the top surface of the disk (the lower node numbers are on the top)

MCODE

-1 indicates the master surface is on the bottom of the disk.

**NBOT** 

Lowest numbered node on the bottom surface. Use only for an eroding interface with MCODE = 1 to detect erosion through the bottom of the plate.

**NLAST** 

= The largest node number which will be on the surface of an eroding interface. See description given for MGEOM = 1.

MGNXT,

 Data for additional master surfaces, described previously for MGEOM = 1.

M1NXT

Master Definition Card for Cylinder Geometry (MGEOM = 4) (415, 15X, 215) — This option can be used if the master surface is on the inside of a hollow cylinder or the outside of a cylinder. The nodal arrangement of the cylinder must be equivalent to that of the rod generator. The first node, M1, is on the lower end of the cylinder as shown in Figure 17. (Higher node numbers are on the lower end.)

NRING

= Nodal ring number of the surface.

NPL

Number of planes of nodes included in the master surface.

IDL

= Node number increment in going from one plane of nodes upward to the next plane. If, for instance, there are 17 nodes per plane, then IDL = -17. IDL is always negative since the increment goes from the higher numbered nodes at the bottom to the lower numbered nodes at the top.

1 indicates the master surface is on the inside of the cylinder. For this option, the first master node, M1, is on the plane of symmetry, on the positive x axis, when the cylinder is in a vertical position about the z axis.

MCODE

-1 indicates the master surface is on the outside of the cylinder.
For this option the first node is on the negative x axes.

MGNXT, M1NXT

 Data for additional master surfaces, described previously for MGEOM = 1.

Master Definition Card for General Geometry (MGEOM = 5) (415) — This option can be used when it is necessary to describe a general master surface which cannot be defined by the other master surface generators (MGEOM = 1, 2, 3, 4). This master surface is defined by a series of individual triangular surfaces, as shown in Figure 17, which are defined in the following card(s). NBOT, NLAST, MGNXT and M1NXT have all been previously defined for MGEOM = 1.

Individual Master Surface Card(s) for MGEOM = 5 (715) — This card describes one or more triangular surfaces which form all or a part of a master surface. Use as many cards as necessary and terminate the series of cards with a blank card.

NCOMP	=	Number of composite groups of triangular surfaces to generate. Each composite group contains one (M4 = 0), two (M4 > 0 and M5 = 0), or four (M5 0) triangles. In Figure 17, NCOMP = 3 for both cases shown.
M1	=	Number of first node. Nodes M1, M2, and M3 must be counterclockwise when viewed from the slave node side of the master surface.
M2	=	Number of second node.
М3	=	Number of third node.
M4	=	Number of fourth node. If $M4=0$ , only one triangle will be generated for each composite group of triangles. If $M4>0$ and $M5=0$ , then $M1$ , $M2$ , $M3$ and $M4$ must be counterclockwise, and two triangles ( $M1$ , $M2$ , $M3$ and $M1$ , $M3$ , $M4$ ) are generated for each composite group, as shown in Figure 17.
M5	=	Number of fifth node. If $M5 = 0$ , only one or two triangles are formed for each composite group of triangles. If $M5 > 0$ , then four triangles are generated for each composite group of triangles, as shown in Figure 17.
INC	=	Node number increment (positive or negative) between corresponding nodes in each composite group of triangular elements. May be left blank for consecutive numbering (INC $= 1$ ).

Slave Node Limits Card for NSN=0 (6E10.0) — All nodes found in or on the box are taken to be slave nodes for the sliding surface. No other slave node cards may be used with this card.

XMAX = Maximum x coordinate of slave node box.
 XMIN = Minimum x coordinate of slave node box.
 YMAX = Maximum y coordinate of slave node box.
 YMIN = Minimum y coordinate of slave node box.
 ZMAX = Maximum z coordinate of slave node box.
 ZMIN = Minimum z coordinate of slave node box.

**NBOX** 

1 will read another Slave Node Limits Card to add another box of slave nodes. Leave blank if there are no more boxes of slave nodes to be added.

# NSG Grouped Slave Node Cards for NSG >0 (315)

S1G

The first node in a group of nodes.

SNG

= The last node in a group of nodes.

INC

= The increment (positive or negative) between the slave nodes. If S1G = 100, SNG = 120, and INC = 5, then nodes 100, 105, 110, 115, 120 will be designated as slave nodes.

Individual Slave Node Cards for NSN > 0 and NSG = 0 (1615) – Individual slave nodes are read if the slave nodes are not consecutive between S1 and SN, and if they are not read in groups (NSG = 0), and if they are not read in by region (NSN > 0).

\$1... SN

= Individual slave nodes read in ascending order.

Restrained Nodes Identification Cards (215, 2X, 311) — Each set of restrained nodes contains one Restrained Nodes Identification Card and additional cards to specify the nodes. The program does not impose any constraint on the number of sets and each set can contain as many as the node arrays can handle. If there are no restrained node sets (NRST = 0 in Miscellaneous Card), this group of cards is omitted. If there is more than one set of restrained nodes, all cards for the first set are entered before the Restrained Nodes Identification Card for the next set is entered. This input redefines the restraints on the designated nodes (it does not simply add to existing restraints). They must be read in ascending order.

NFN

Number of nodes in set.

**NFG** 

Number of groups of nodes to be read. If NFG = 0 the nodes are read individually.

IX, IY, IZ

= 1 restrains nodes in X, Y, Z directions, respectively. Expanded description given for Line of Nodes Description Card in Node Geometry Subsection.

# Individual Restrained Nodes Cards - For NFG = 0 (1615) -

F1...FN = Individual nodes to be restrained in ascending order.

# NFG Group Restrained Nodes Cards (315) -

F1G = First node in the group of nodes to be restrained.

FNG = Last node in the group of nodes to be restrained. (May be zero if

there is only one node in the group.)

INC = Increment between nodes in the group of restrained nodes. (May

be zero if the increment is one or if no increment is needed.)

Detonation Card (4F10.0) - Leave card blank if no explosives are used.

XDET = x coordinate of detonation for high explosive (distance).

YDET = y coordinate of detonation (distance).

ZDET = z coordinate of detonation (distance).

TBURN = Time at which the detonation begins at XDET, YDET, ZDET.

Initial Velocity Card (7E10.0) — This card describes the initial velocity conditions of the projectile and the target. If there are interface nodes which include mass from both the projectile and the target, the velocities of these nodes are adjusted by the program to conserve momenta.

PXDOT = Projectile velocity in the x direction (distance/time).

PYDOT = Projectile velocity in the y direction.

PZDOT = Projectile velocity in the z direction.

TXDOT = Target velocity in the x direction.

TYDOT = Target velocity in the y direction.

TZDOT = Target velocity in the z direction.

DT1 = Integration time increment for the first cycle. This must be less

than the time required to travel across the minimum altitude of each tetrahedral element at the sound speed of the material in

that element.

#### a. Material Descriptions

**IFAIL** 

**DFRAC** 

**EFAIL** 

A summary of input data for material descriptions is given in Figure 2. Four material types are available: solids, explosives, crushable solids and anisotropic solids.

Material Cards for Solids from Library (415, 2F5.0) — Data for some materials are available from the material library in subroutine MATLIB. The specific materials are listed as output from the Preprocessor. Library materials may be used directly without being called by this card. If they are called by this card, however, the material data will be printed as part of the output. This card also allows the user to make some decisions regarding fracture options. The user should read the comments in subroutine MATLIB to obtain the references from which the data were generated.

MATL	=	Material identification number. It must be in the range of 1 through 50 and must correspond to a material number in the library.
0	=	Code to specify library material

IDAM = 1 will compute material damage. The option in the library is IDAM = 0, which will not compute damage.

0 will not allow failure of the material when the damage exceeds 1.0, but rather will continue to accumulate the damage. This is the option which is in the library.

1 will allow the material to fracture partially when the damage exceeds 1.0. Partial fracture causes shear and tensile failure, so only compressive hydrostatic pressure capability remains.

Factor by which library fracture strain constants (D1, D2, EFMIN – defined later) are multiplied. If left blank, (DFRAC = 0) factor will be set to DFRAC = 1.0.

Equivalent plastic strain (or volumetric strain), which, if exceeded, will totally fail the element such that it produces no stresses or pressures. If left blank, the library values of EFAIL = 999 will govern.

Five Material Cards for Solid Input Data [415, 5X, F5.0, A48/4(8F10.0)] — These five cards specify all the material constants for a solid material. These cards will supersede any material library data with the same material number, MATL. Only previously undefined variables will be defined.

**DENSITY** = Material density (mass/volume).

SPH HEAT = Specific heat (work/mass/degree).

CONDUCT = Thermal conductivity (power/distance/degree).

ALPHA = Volumetric coefficient of thermal expansion (degree $^{-1}$ ).

TEMP1 = Initial temperature of the material (degree).

TROOM = Room temperature (degree).

TMELT = Melting temperature of the material (degree).

X1 = Extra material constant stored in the C9 array (not currently used).

SHEAR MOD = Shear modulus of elasticity (force/area).

C1, C2, N, C3, = Constants to describe the material strength,  $\sigma$ . The primary form of the M, C4, SMAX strength equation is

$$\sigma = [C1 + C2 \cdot \epsilon^{N}][1 + C3 \cdot \ell n \dot{\epsilon}^{*}][1 - T^{*M}] + C4 \cdot P$$
 (1)

Where  $\epsilon$  is the equivalent plastic strain,  $\dot{\epsilon}^* = \dot{\epsilon}/\dot{\epsilon}_0$  is the dimensionless strain rate for  $\dot{\epsilon}_0 = 1.0 \text{ s}^{-1}$ , T\* is the homologous temperature, and P is hydrostatic pressure (compression is positive). N must be a positive number, and the thermal softening fraction,  $K_T = [1 - T^{*M}]$ , is set to  $K_T = 1.0$  when M = 0. If SMAX is input as a positive number, then the maximum strength for  $\sigma$  is limited to SMAX. If left blank (SMAX = 0) the strength ( $\sigma$ ) is not limited. A more detailed description of the strength model and data is given in Reference 4.

A constant flow stress can be obtained by setting C1 to the flow stress, N = 1.0, and C2 = C3 = C4 = SMAX = M = 0. C1, C2 and SMAX have units of stress (force/area) and the others are dimensionless.

K1, K2, K3 = Cubic coefficients for the Mie-Gruneisen equation of state (force/area)

$$P = (K1\mu + K2\mu^2 + K3\mu^3)(1 - \Gamma\mu/2) + E_{s}(1 + \mu)$$
 (2)

where  $\mu = \rho/\rho_0 - 1$  and  $E_s$  is internal energy per initial volume.

 $\Gamma$  = Gruneisen coefficient for Mie-Gruneisen equation of state.

CL = Linear artificial viscosity coefficient (CL ≈ 0.2).

CQ

= Quadratic artificial viscosity coefficient (CQ ≈ 4.0).

**PMIN** 

Maximum hydrostatic tension allowed (force/area).

CH

= Hourglass artificial viscosity coefficient for quad elements (CH ≈ 0.02).

D1...D5

= Constants for the fracture model (Reference 6).

$$\epsilon^{f} = [D1 + D2\exp^{D3\sigma*}][1 + D4 \cdot \ell n \dot{\epsilon}^{*}][1 + D5 \cdot T^{*}]$$
(3)

Where  $\epsilon^f$  is the equivalent strain to fracture under constant conditions of the dimensionless strain rate,  $\dot{\epsilon}^*$ , homologous temperature,  $T^*$ , and the pressure-stress ratio,  $\sigma^* = \sigma_m/\bar{\sigma}$ . The mean normal stress is  $\sigma_m$  and  $\bar{\sigma}$  is the von Mises equivalent stress. Expression is valid for  $\sigma^* \leq 1.5$ . Damage is computed from  $D = \Sigma \Delta \epsilon/\epsilon^f$ , and fracture is allowed to occur when D = 1.0.

**SPALL** 

= Tensile spall stress (negative pressure) at which fracture can occur (force/area).

**EFMIN** 

= Minimum fracture strain allowed. For  $\sigma^* > 1.5$ ,  $\epsilon^f$  varies linearly from  $\epsilon^f$  at  $\sigma^* = 1.5$  to EFMIN at  $\sigma_m = \text{SPALL}$ 

**X**2

= Extra material constant stored in the C10 array.

Material Cards for Explosives from Library (215) — Similar to the cards for the solid materials in the library except that no options are provided for fracture.

Three Material Cards for Explosives Input Data (215, 20X, A48/6F10.0/7F10.0) — Only new variables will be defined. See solid material definitions for other variables.

**ENERGY** 

= Initial internal energy in explosive,  $E_0$  (energy/volume).

DET VEL

Detonation velocity, D (distance/time).

C1...C5

= Constants for the JWL equation of state. If left blank, a gamma law equation of state is used where

$$\gamma = \sqrt{1 + D^2 \rho / 2E_0} \tag{4}$$

For gamma law the pressure is determined from

$$P = (\gamma - 1)E/\overline{V}$$
 (5)

For JWL the pressure is determined from

$$P = C1 \cdot (1-C5/C2 \overline{V}) \cdot \exp(-C2 \cdot \overline{V}) + C3 \cdot (1-C5/C4 \overline{V}) \cdot \exp(-C4 \cdot \overline{V}) + C5 \cdot E/\overline{V}$$
(6)

where E is internal energy per initial volume and  $\nabla = V/V_0$  is the relative volume. C1 and C3 have the units of pressure (force/area) and C2, C4, C5 are dimensionless.

X1, X2

Extra material variables stored in arrays C6 and C7.

Material Cards for Crushable Solids from Library (215, 15X, F5.0) — These cards are similar to the cards for other library materials. Total failure is allowed through EFAIL, but fracture due to damage is not allowed.

Four Material Cards for Crushable Solids Input Data [215, 15X, F5.0, A48/3F10.0/2(8F10.0)] — These four cards specify the material constants for a crushable solid material (Reference 5). Only new variables will be defined. See previous material definitions for other variables.

C1, C4 = Constants to describe the material strength,  $\sigma$ .

$$\sigma = C1 + C4 \cdot P \tag{7}$$

SMAX = Maximum strength allowed (force/area). If left blank (SMAX = 0), strength  $(\sigma)$  is not limited.

PCRUSH, = Constants to describe the pressure, P. The model, UCRUSH, and specific data for concrete, are shown in Figure K1, K2, K3, 18. The basic model can also be used for other crushable solid materials. PCRUSH, K1, K2, K3 and ULOCK KLOCK have units of pressure (force/area). UCRUSH

and ULOCK are dimensionless.

X1 = Extra material constant stored in the D1 array.

Eight Material Cards for Each Anisotropic Material [415, 5X, F5.0, A48/3F10.0/2(6F10.0)/ 2(8F10.0)] — Some special comments are as follows: If K1 = 0 an isotropic pressure,  $P^*$ , is determined from the linear elastic constants. For this option, there are no energy effects and the pressure is defined by

$$P = P^* + K2\mu^2 + K3\mu^3$$

where K2 and K3 are isotropic coefficients and  $\mu = \rho/\rho_0$ -1. Generally, one should set K2 = K3 = 0 since there is no sound basis for higher order isotropic pressure terms in anisotropic materials. If K1 = 0 and  $\Gamma$  = 0, P\* is computed directly from the strains and is valid only for small strains. If K1 = 0 and  $\Gamma$  = 1.0, P\* is computed incrementally and large strains can be accommodated If incremental pressures are determined for elements containing nodes on a sliding surface, errors can be introduced if the displacements are not consistent with the velocities. This can occur if there is not a good velocity match on the sliding surface. Also, for K1 = 0 and  $\Gamma$  = 1.0, no external pressures can be applied since an external pressure array is used to store P\* between cycles. For K1 > 0, the isotropic Mie-Gruneisen Equation of State is used for the pressure. This option can be used if it is desirable to include energy effects in the pressure computation.

 $\theta_1, \theta_2, \theta_3$  = Euler angles between the system axes and the material axes. The material input data to follow should be relative to the system coordinate axes. If its initial orientation does not coincide with the system axes, then the Euler angles are used to define the initial orientation. See Figure 19 for definition of the angles. For an anisotropic rod which is rotated from vertical to 30 degrees from vertical, ( $\theta_y = -30$  degrees in x-z plane) the corresponding Euler angles are  $\theta_1 = 90^{\circ}$ ,  $\theta_2 = -30^{\circ}$  and  $\theta_3 = -90^{\circ}$ .

 $\nu_{xy}$ ,  $\nu_{yz}$ ,  $\nu_{zx}$  = Three Poisson's ratios. Note that  $\nu_{xy}$  is defined as the relative decrease in the y direction due to a tensile increase in the x direction.

 $E_x$ ,  $E_y$ ,  $E_z$  = Moduli of elasticity in the three principal directions.

 $G_{xy}$ ,  $G_{yz}$ ,  $G_{zx}$  = Shear moduli of elasticity in the three principal planes (force/

area).

X-YIELD = Tensile flow stress in the x direction (force/area).

Y-YIELD = Tensile flow stress in y direction.

Z-YIELD = Tensile flow stress in z direction.

XY-YIELD = Shear flow stress in the x-y plane (force/area).

YZ-YIELD = Shear flow stress in y-z plane.

ZX-YIELD = Shear flow stress in z-x plane.

It should be noted that the algorithm to find the yield surface may not converge if the individual tensile flow stresses (or individual shear stresses) vary by more than a factor of 1.5 to 2.5. When this occurs, an approximate radial return method is used and a warning message is printed in the cycle output data.

### b. Node Geometry

A summary of input data for nodal geometry is given in Figure 3. Nodes may be input as a line of nodes, and/or special shapes consisting of rods, various nose geometries, flat plates and spheres. There is no limit to the number of shapes included for the projectile or the target. In all cases the nodes are numbered consecutively. If a node is at the interface of the projectile and the target and contains mass from both the projectile and the target, it must be included with the projectile nodes.

Line of Nodes Description Card (215, 6F10.0, F7.0, 311) — One card is required for each line of nodes to be generated. Refer to Figure 8 for the spacing of the nodes.

1 = Identification number for line of nodes geometry.

NNODE = Number of nodes in the row of nodes. The nodes are numbered consecutively.

consecutively.

X1 = x coordinate of first node (distance).

Y1 = y coordinate of first node (distance).

z coordinate of first node (distance).

XN = x coordinate of last node (distance). Leave blank if a single node is

entered.

YN = y coordinate of last node (distance).

ZN = 2 coordinate of last node (distance).

EXPAND = Factor by which the distance between nodes is multiplied going from the first node to the last node. Leave blank for uniform

spacing.

IX = 1 will restrain all nodes (N1...NN) in the x direction. No restraint

if left blank.

IY = 1 will restrain nodes in y direction.

IZ = 1 will restrain nodes in z direction.

Rod Node Identification Card (15) — The rod shape geometry descriptions are given in Figure 11. The rod is always generated in a vertical position about the z axis. When viewed from the positive z direction, the nodes are numbered consecutively counterclockwise, inner to outer and downward. Only one-half the rod is generated as shown, and restraints are provided normal to the plane of symmetry. The rotation of the rod for oblique impact is obtained with a Scale/Shift/Rotate Card.

2 = Identification number for rod nodes geometry.

# Rod Node Description Card (415, 3F10.0) -

NOR = Outer node ring number.

NIR = Inner node ring number. The inner node ring number for a solid

rod is 0.

NPLN = The number of cross-sectional planes of nodes in the rod.

0 gives uniform radial spacing and constant z coordinates at the

top and bottom of the rod.

1RAD = 1 requires all r and z coordinates at top and bottom of rod to be

input individually.

ZTOP = The constant z coordinate of the top of the rod for IRAD = 0, or the

top centerline z coordinate (if applicable) for IRAD = 1.

ZBOT = The constant z coordinate at the bottom of the rod for IRAD = 0,

or the bottom centerline z coordinate (if applicable) for IRAD = 1.

EXPAND = Factor by which the distance between corresponding nodes in the

vertical direction is multiplied going from top to bottom. Leave

blank for uniform spacing in the vertical direction.

### Rod Node Radii Card for IRAD = 0 (4F10.0) -

ROTOP = Outer radius of the rod top.

RITOP = Inner radius of the rod top.

ROBOT

Outer radius of the rod bottom.

RIBOT

Inner radius of the rod bottom.

### Rod Node Top Radii Card(s) for IRAD = 1 (8F10.0) -

RT(I)

= Top radii for each node ring (I = NIR, NOR). Array RT is currently dimensioned for a maximum outer ring number of 16. If NIR = 0, then RT(0) internally set to 0 and I = 1, NOR.

# Rod Node Bottom Radii Card(s) for IRAD = 1 (8F10.0) -

RB(I)

Bottom radii for each node ring (I = NIR, NOR). Array RB is currently dimensioned for a maximum outer ring number of 16. If NIR = 0, then RB(0) internally set to 0 and I = 1, NOR.

### Rod Node Top Surface Card(s) for IRAD = 1 (8F10.0) -

ZT(I)

= Top z coordinate for each node ring (I = NIR, NOR). If NIR = 0 then ZT(0) = ZTOP in the Rod Node Description Card and I = 1, NOR. Note that the top z coordinates do not all have to be equal as shown in Figure 11, but can be varied to form curved surfaces.

### Rod Node Bottom Surface Card(s) for IRAD = 1 (8F10.0) -

ZB(I)

Bottom z coordinate for each node ring (I = NIR, NOR). If NIR = 0, then ZB(0) = ZBOT in the Rod Node Description Card and I = 1, NOR.

NOTE: If it is not possible to describe the node geometry of the rod with a single shape, it is possible to use multiple shapes to form a single rod. The nodes must be numbered consecutively, and the radii and the number of node rings must be the same for the individual rod shapes at their interface. Also, ZBOT and ZTOP for adjoining rods should not be identical. ZTOP for the lower rod should be less than ZBOT for the upper rod by the desired node spacing in the z direction.

Nose Node Identification Card (15) — The nose geometry descriptions are given in Figure 12. The nose shape is always generated in a vertical position (pointed downward) about the z axis. When viewed from the positive z direction, the nodes are numbered consecutively, counterclockwise, downward, and inner to outer. Only one-half the nose shape is generated as shown, and restraints are provided normal to the plane of symmetry. The node geometry for the plane of nodes at the rod interface is not generated with the nose generator and must therefore be generated with the rod generator. The number of rings must be identical for the rod and the nose.

= Identification number for nose geometry.

#### Nose Node Description Card (4I5, 4F10.0) -

NOR

3

= Outer node ring number.

NIR

= Inner node ring number.

1 identifies a conical nose shape.

**INOSE** 

2 identifies a rounded nose shape. If the length of the nose is equal to the radius, a spherical shape is generated. When the length is not equal to the radius, the axial coordinates are scaled and the various radii are not changed.

3 identifies a tangent ogival nose shape.

**IRAD** 

= Radius option. If IRAD = 1, individual radii and z coordinates are input for each ring of nodes. Leave blank (IRAD = 0) for uniform spacing.

ROTOP

= Top outer node radius of nose.

**RITOP** 

Top inner node radius of nose.

**ZTOP** 

The z coordinate at the top of the nose. This is identical to ZBOT for the rod interface.

**ZMIN** 

= The z coordinate at the tip of the nose.

# Nose Node Top Radii Card(s) for IRAD = 1 (8F10.0) -

RT(I)

Top radius for each node ring (I = NIR, NOR). Array RT is currently dimensioned for a maximum outer ring number of 16. If NIR = 0, then RT(0) internally set to 0 and I = 1, NOR.

### Nose Node ZMIN Card(s) for IRAD = 1 (8F10.0) -

ZM(I)

= Minimum coordinates for each node ring (I = NIR, NOR). Array ZM is currently dimensioned for a maximum outer ring number of 16. If NIR = 0, then ZM(0) internally set to ZTOP and I = 1, NOR.

Flat-Plate Node Identification Card (215) — The flat-plate descriptions are given in Figure 13. In all cases, the lines connecting the adjacent corner nodes are parallel to one of the three primary axes. The nodes are generated in rows parallel to the x axis and are numbered consecutively within each row in the direction of the increasing x axis. The TYPE = 1 option generates the nodes in horizontal planes, row by row in the positive y direction and plane by plane in the negative z direction. The TYPE = 2 option generates the nodes in vertical planes; row by row in the negative z direction and plane by plane in the positive y direction. This TYPE = 2 option can sometimes be used to minimize the nodal bandwidth for penetration into thick plates.

4

= Identification number for flat-plate geometry.

**TYPE** 

= \begin{cases}
1 generates nodes in horizontal planes \\
2 generates nodes in vertical planes

Flat-Plate Node Description Card for TYPE = 1 (615, 5F10.0) - This option generates nodes in horizontal planes. The following descriptions refer to the upper portion of Figure 13.

NX = The number of nodes in the x direction; in Figure 13, NX = 13.

NY = The number of nodes in the y direction; in Figure 13, NY = 7.

NZ = The number of nodes in the z direction; in Figure 13, NZ = 5.

direction.

NXEND = The number of nodes in the x direction in each of the two variable x spacing regions. The node at the division between the uniform and the variable spacing sections is included in this number. The spacing is determined by X-EXPAND and the fractional length by X-PART. In Figure 13, NXEND = 4. Depending on whether NX is odd or even, NXEND can have a maximum value of either (NX + 1)/2 or NX/2, respectively, unless the special option discussed in X-PART is used. The remaining middle x region (if any) is uniformly spaced. Leave blank for uniform spacing in the x

The number of nodes in the y direction in the variable y spacing region. The node at the division between the uniform and the variable spacing sections is included in this number. Spacing is determined by Y-EXPAND and the fractional length by Y-PART. In Figure 13, NYEND = 4. NYEND can have a maximum value of NY. The remaining y region (if any) is uniformly spaced. Leave blank for uniform spacing in the y direction.

= 1 gives restraint in the y direction only if y = 0 (Y1 = 0.0).

= Factor by which the x distance between adjacent nodes changes outward to the ends for each X-PART variable spacing region. Same as described for the Line of Nodes Description Card.

= Fractional part of the total x length of the flat plate occupied by each of the variable x spacing regions. If X-PART = 0.0, the entire spacing in the x direction is uniform. If X-PART = 0.5 and NXEND = NX/2, the spacing in the positive x direction is variable for entire x length (X1 to XN).

= Factor by which the y distance between adjacent nodes changes in the increasing y direction for the Y-PART variable spacing region.

= Fractional part of the total y length of the flat plate occupied by the variable y spacing region.

NYEND

ſΥ

X-EXPAND

X-PART

**Y-EXPAND** 

**Y-PART** 

**Z-EXPAND** = Factor by which the z distance between adjacent nodes changes in the decreasing z direction from Z1 to ZN.

Flat Plate Node Description Card for TYPE = 2 (615, 5F10.0) - This option generates nodes in vertical planes. See lower portion of Figure 13 for description. Definition of variables is analogous to those of the TYPE = 1 variables.

# Flat-Plate Node Size Card (6F10.0) -

X1 = The minimum x coordinate of the plate shape.

Y1 = The minimum y coordinate of the plate shape.

Z1 = The maximum z coordinate of the plate shape.

XN = The maximum x coordinate of the plate shape.

YN = The maximum y coordinate of the plate shape.

ZN = The minimum z coordinate of the plate shape.

Sphere Node Identification Card (15) — The cross section of the bottom spherical shape is identical to that shown for the rounded nose shape of Figure 12. The top one-half cross section is initially geometrically symmetric to the bottom. Only one-half of the top and bottom halves are generated, and restraints are provided normal to the vertical plane of symmetry. The sphere is generated with the nodes numbered as two rounded circular noses having an interface between. The top nose is generated first; viewed from the positive z direction, this generation is counterclockwise, upwards and inner to outer. The bottom nose is generated with the interface included with each spherical shell; this generation viewed from the positive z direction is counterclockwise, downwards and inner to outer. A summary of the number of nodes included in the various shapes is given in Figure 16.

5 = Identification number for sphere geometry.

# Sphere Node Description Card (215, 5X, 15, 3F10.0) -

NOR = Outer node ring number.

NIR = Inner node ring number.

IRAD = 0 gives RO, RI, ZCG input option for uniform spacing.

1 gives RT(I), ZCG input option (I = NIR, NOR).

RO = Radius of outer node ring.

RI = Radius of inner node ring.

ZCG = The z coordinate of the center of the sphere.

# Sphere Node Radii Card(s) for IRAD = 1 (8F10.0) -

RT(I)

= Radii for each node ring (I = NIR, NOR). Array RT is currently dimensioned for a maximum outer ring number of 16. If NIR = 0, then RT(0) internally set to 0 and I = 1, NOR.

NABOR Filled Plate Node Identification Card (15) — Generates nodes for a plate with normal (tetrahedral element) edges and NABOR nodes in the center, as shown in Figure 14, so that penetration problems can have NABOR nodes in the high distortion region and normal elements in the low distortion region. Limited to generating the +Y half of mirror symmetry about Y=0. The node generation is generally from the center of the plate to the edge. The nodes are generated in a column at a fixed X and Y from the largest Z to the smallest (or most negative) Z. The NABOR nodes are generated first. The column at X=(X1+XN)/2, Y=DO/2 is generated first followed by the other interior NABOR nodes. The exterior layer of NABOR nodes and all the normal nodes are generated in columns in a generally counterclockwise direction. The mass of the NABOR nodes is dependent only on the density of the material and the diameter of the NABOR nodes. They cannot accept mass from attached elements. The diameters of all NABOR nodes in a specific problem must be identical.

The size of the NABOR node region can be calculated from the number of NABOR nodes in each direction and their diameter. See Figure 14 for a typical example. The z dimension has the NABOR nodes stacked in columns but alternate columns are offset by half a diameter. The depth in the z direction is (NNZ+0.5)\*DO. The y dimension consists of layers of NABOR nodes. The separation between the layers is only SQRT (2/3)\*DO which makes the y width ((NNY-1)\*SQRT(2/3)+1)\*DO. The x dimension has both layers and an offset. The distance between columns in the x direction is SQRT(3/4)\*DO. The offset between layers is (SQRT(1/12))\*DO. The x width is (NNX\*SQRT(3/4)+SQRT(1/12))\*DO.

6 = Identification number for NABOR filled plate geometry.

### NABOR Filled Plate Node Description Card (715, 5X, 3E10.0) -

NNX	=	Number of NABOR nodes in the x direction. This number must be 3 or larger and odd. In Figure 14, $NNX = 7$ .
NNY	=	Number of NABOR nodes in the y direction. This number must be 3 or larger and odd. In Figure 14, NNY = 5.
NNZ	=	Number of NABOR nodes in the z direction. This number must be 2 or larger. In Figure 14, NNZ = 3.
MATL	=	Material number for plate. Used for NABOR nodes.
NXEND	=	Number of normal nodes on each end in the x direction. In Figure 14, $NXEND = 3$ .
NYEND	=	Number of normal nodes on the positive y side of the plate. Both NXEND and NYEND must be zero or nonzero together. In Figure 14, NYEND = 3.

IY = 1 gives restraint in the y direction if Y1 = 0.

X-EXPAND = Factor by which the x distance between adjacent nodes changes

for the regular (not NABOR) nodes.

Y-EXPAND = Factor by which the y distance between adjacent nodes changes

for the regular nodes.

DO = Diameter of the NABOR nodes. The first DO read must be positive. Following DOs may be the same value or the field can be left

blank.

# NABOR Filled Plate Size Card (5E10.0) -

X1 = The minimum x coordinate of the plate.

Y1 = The minimum y coordinate of the plate. When NYEND > 0 then

Y1 must be 0.0.

ZTOP = The maximum z coordinate of the plate.

The maximum x coordinate of the plate. The middle column in the plane of nodes which touches the y = Y1 plane is generated at (X1+XN)\*0.5. When NXEND > 0, then the width (XN-X1) must be larger than (NNX+4)\*SQRT(3/4)\*DO. When NXEND=0, then the plate is all NABOR nodes and the width has already been

determined.

YN = The maximum y coordinate of the plate. When NXEND > 0, the width (YN) must be larger than (NNY+2)\*SQRT(2/3)\*DO. When NXEND=0, then the plate width has already been determined

and YN is ignored.

The minimum Z coordinate value is ZBOT = ZTOP - (NNZ + 0.5)\*DO.

NABOR Brick Node Identification Card (15) — This option generates a brick shape composed entirely of NABOR nodes as shown in Figure 15. It generates the largest NABOR brick which lies completely within the specified size. The NABOR nodes touch the X1, Y1, Z1, planes but may not reach to the XN, YN, ZN planes.

7 = Identification number for NABOR brick geometry.

# NABOR Brick Node Description Card (215, E10.0) -

MATL = Material number for NABOR nodes.

IY = 1 gives restraint in the y direction if Y1 = 0.

DO = Diameter of the NABOR nodes. The first DO read must be positive. Following DOs may be the same value or the field can be left blank.

**X1** The minimum x coordinate of the brick shape.

**Y**1 The minimum y coordinate of the brick shape.

 $\mathbf{Z}_{\mathbf{1}}$ The maximum z coordinate of the brick shape.

XN The maximum x coordinate of the brick shape.

YN The maximum y coordinate of the brick shape.

ZN The minimum z coordinate of the brick shape.

#### c. Element Geometry

A summary of input data for element geometry is given in Figure 4. Elements may be input as a series of individual or composite elements and/or special shapes of rods, nose geometries, flat plates, and/or spheres. The elements must be assembled in a manner consistent with the previously generated nodal geometry. There is no limit to the number of shapes included for the projectile or the target.

Series of Composite Elements Description Card (1215) - Element cards for each Series of Composite Elements are supplied as needed by the user. For this discussion it will be assumed that the elements are entered as a series of composite brick elements, each containing six individual elements as shown in Figure 9. Following this immediate discussion will be an example and instructions for generating a series of individual elements.

1 = Identification number for a series of composite elements.

**NCOMP** Number of composite elements in the series.

MATL = Material number of the elements. If left blank, the material number from the previous element data card will be used.

N1-N8 = Node numbers of the first composite brick element as shown in Figure 9. Nodes N1, N2, N3, N4 and nodes N5, N6, N7, N8 are

counterclockwise when looking from N1 to N5.

INC The node number increment added to the node numbers of the previous composite brick element for the next composite brick

element.

An example of input data for composite brick elements is shown in Figure 10. In the upper left it can be seen that there are four rows of nodes (1 to 4, 5 to 8, 9 to 12, 13 to 16), which are arranged to contain three composite brick elements. If the first element is numbered 1, then the first composite brick contains elements 1 to 6, the second contains 7 to 12, and the third contains 13 to 18. The first composite brick is defined by nodes N1 = 1, N2 = 5, N3 = 9, N4 = 13, N5 = 2, N6 = 6, N7 = 10, and N8 = 14. Note that N1 to N4and N5 to N8 are counterclockwise when looking from N1 to N5. The six individual elements are generated according to the arrangement and order (A, B, C, D, E, F) shown in

Figure 9. The node numbers for each successive brick are simply INC = 1 greater than those of previous brick. For the second brick, for instance, N1 = 1 + 1 = 2, N2 = 5 + 1 = 6, N3 = 9 + 1 = 10, N4 = 13 + 1 = 14, N5 = 2 + 1 = 3, N6 = 6 + 1 = 7, N7 = 10 + 1 = 11, and N8 = 14 + 1 = 15.

It is possible to generate a series of individual tetrahedral elements by letting N1 to N4 be the nodes of the first element, where N1, N2, and N3 are counterclockwise when viewed from N4. This option is exercised when N5 to N8 are left blank. It is also possible to generate a series of composite wedge elements, each containing three individual tetrahedral elements. The three elements in a composite wedge element are numbered consecutively. If N2 and N6 are left blank, the first three tetrahedron elements (A, B, C) are defined by nodes N1, N3, N4, N5, N7 and N8 as shown in Figure 9. Likewise, if N4 and N8 are left blank, the first three elements (D, E, F) are defined by nodes N1, N2, N3, N5, N6, and N7. Do not use composite wedge elements or individual tetrahedral elements in conjunction with the average pressure option (VRFACT) described in the Main Routine.

Rod Element Identification Card (15) — Elements are generated for the rod shapes illustrated in Figure 11 and described by the Rod Shape Node Cards. The elements are numbered consecutively and are generated in layers of composite brick elements beginning with top layer 1 and ending at bottom layer NLAY. The entire first layer of elements is generated before the second layer, etc., and the composite brick elements of each layer are generated in a counterclockwise manner for each ring of elements from the inner to the outer ring.

2 = Identification number for rod geometry.

# Rod Element Description Card (515) -

N1

MATL

NOER = Outer element ring number.

NIER = Inner element ring number. The inner element ring number for a

solid rod is 1.

NLAY = The number of layers of elements in the rod. The total number of elements in a rod shape shown in Figure 11 is dependent on the

number of layers and the number of elements per layer. The number of elements per layer is dependent on the inner and outer element ring numbers. [For example: If NLAY = 10, NIER = 2 and NOER = 5, the total number of elements can be determined through use of Figure 16. The number of elements per layer for the solid rod of NOER = 5 is 300, and of NIER = 2 is 48. Therefore,

the total of elements for the hollow cylinder is 10(300-48) = 2520.

The number of the lowest numbered rod node. For the solid rod, this is the centerline node on the top end of the rod. For the hollow rod, this is the innermost clockwise node on the top end of the rod

when viewed from the top.

= Material number of a uniform material rod. MATL = 0 gives M(I) input option (I = NIER, NOER), where material numbers for each

element ring must be input individually.

### Rod Element Material Card for MATL = 0 (1615) -

M(I)

Material number for each element ring (I = NIER, NOER). Array
 M is currently dimensioned for a maximum outer ring number of
 16.

Nose Element Identification Card (15) — Elements are generated for the nose shapes illustrated in Figure 12 and described by the Nose Shape Node Cards. The elements are numbered consecutively and are generated in shells of composite brick elements beginning with the innermost shell and ending with the outermost shell. The entire first shell of elements is generated before the second shell, etc., and the composite brick elements of each shell are generated in a counterclockwise manner for each ring of elements from the top to the bottom of each shell.

3

= Identification number for Nose Geometry.

### Nose Element Description Card (215, 5X, 215) -

NOER

Outer element ring number.

**NIER** 

= Inner element ring number.

N<sub>1</sub>

 The number of the lowest numbered nose node. (The nose does not include interface nodes.)

MATL

Material number of a uniform material nose. MATL = 0 gives M(I) input option (I = NIER, NOER), where material number for each element ring must be input individually.

# Nose Element Material Card for MATL = 0 (1615) -

M(I)

Material number for each element ring (I = NIER, NOER). Array
 M is currently dimensioned for a maximum outer ring number of
 16.

Flat-Plate Element Identification Card (215) — The elements are generated for the flat-plate illustrated in Figure 13 and described by the Flat-Plate Shape Node Cards. The elements are numbered consecutively and are generated in rows of composite brick elements. The rows of elements go in the direction of the increasing x axis. The TYPE = 1 option generates the elements in horizontal layers and the TYPE = 2 option generates the elements in vertical layers. Element generation must be consistent with the generation of nodes.

4

Identification number for flat-plate geometry.

TYPE

1 generates elements in horizontal layers.
2 generates elements in vertical layers.

# Flat-Plate Element Description Card (515) -

NLX Number of layers of composite brick elements in the x direction. The total number of nodes along the x direction must be NLX + 1.

In Figure 13, NLX = 12.

NLY = Number of layers of composite brick elements in the y direction. The total number of nodes along the y direction must be NLY + 1.

In Figure 13, NLY = 6.

NLZ = Number of layers of composite brick elements in the z direction. In

Figure 13, NLZ = 4.

N1 = The node number of the corner node shown in Figure 13.

MATL = Material number of the flat plate.

Sphere Element Identification Card (15) - Elements are generated for a sphere, the bottom half cross section of which is identical to the rounded nose shown in Figure 12 and described by the Sphere-Shape Nose Cards. When viewed from the top, the elements are consecutively numbered counterclockwise, upwards and outwards for the top one-half and then counterclockwise, downwards and outwards for the bottom one-half.

5 = Identification number for sphere shape.

# Sphere Element Description Card (215, 5X, 215) -

NOER = Outer element ring number.

NIER = Inner element ring number. The inner element ring number for a

solid sphere is 1.

N1 = The number of lowest numbered sphere node.

MATL = Material number of a uniform material sphere. MATL = 0 gives M(I) input option (I = NIER, NOER), where material number for

each element ring must be input individually.

### Sphere Element Material Card for MATL = 0 (1615) -

6

= Material number for each element ring (I = NIER, NOER). Array M(I)M is currently dimensioned for a maximum outer ring number of 16.

NABOR Filled Plate Element Identification Card (15) - Elements are generated for the plate surrounding the NABOR nodes, as shown in Figure 14. The inner element layer is generated between the outer layer of NABOR nodes and the first inner layer of normal nodes. The order of generation is similar to the generation of the normal nodes, in layers of columns and generally counterclockwise.

= Identification for NABOR filled plate shape.

# NABOR Filled Plate Element Description Card (715) -

NNX NNY NNZ MATL NXEND NYEND

= Identical to input used for corresponding NABOR filled plate node description card.

N1

The number of the lowest numbered NABOR node in the plate.

#### 2. INPUT DATA FOR THE MAIN ROUTINE

The function of the Main Routine is to perform the computations. The Main Routine reads initial conditions from the restart tape which must be generated from a Preprocessor run or a previous Main Routine run. The descriptions that follow are for the data in Figure 5. Consistent units must be used.

It is possible to interject user comments into the data by use of a \$ character, as described for the Preprocessor.

**Description Card (A80)** – A description of the problem provided by the user.

### Identification Card (515, 5X, 5F10.0) -

**CASE** 

Case number for run identification.

**CYCLE** 

= The cycle number at which the restart occurs. The cycle numbers for which restart files are written are given in the printed output of the previous run (Preprocessor or Main Routine).

0 gives no applied pressures read or applied.

**IPRES** 

1 will use the pressure data which was input in a previous run.

2 will read applied pressures to be used in subsequent computations.

0 will not allow problem size to be changed.

1 will allow the problem to be reduced in size at a specified time.

**CHANG** 

2 will allow the problem size to be reduced at one time, and then increased at another time. The expansions and reductions can be performed in either order. If identical times are designated for the expansion and reduction, the reduction will be performed first.

3 will allow the problem size to be expanded at a specific time.

IHRG

= 1 will use hourglass artificial viscosity when computing brick average pressures for solid materials. Generally not required.

#### **VFRACT**

Fraction of initial volume of a brick at which individual element pressure is computed. An average pressure is computed for a brick volume larger than VFRACT. Average pressures are not used if VFRACT = 0 or the field is blank. Expanded description given in Reference 8. Use of VFRACT option requires all elements to be input with special shape generators or composite brick elements. No wedges or individual tetrahedral elements are allowed.

#### **PMAX**

Maximum pressure allowed in any element. Pressure not limited if PMAX = 0 (or blank field).

#### **VNREF**

Reference closing velocity for NABOR search routines. It should be 0.2 to 1.0 times the impact velocity (or relative closing velocity) in the problem. Lower values will cause less searching but may allow two NABOR nodes to become too close before being detected. Higher values will cause more searching but will also ensure that nodes do not become too close before being detected.

#### ARMAX

= For anisotropic materials the maximum angle an element can rotate (in degrees) before recalculating the element axes. A properly chosen value can significantly reduce central CPU time with only a small loss of accuracy. A large value will prevent recalculating element rotations, which will cause all elements to be treated as if they did not rotate. This uses the minimum CPU time and may be suitable for some problems. A small value of ARMAX = 1.0 degree will bypass the lengthy element axis calculation for elements in regions where the nodes do not have significant rotations.

#### **ASERR**

= The maximum relative error allowed when calculating the stress at the yield surface for anisotropic materials. The acceptable band of stresses is from 1.0-ASERR to 1.0+ASERR times the actual yield stress. When left blank, the value of ASERR = 0.01 will be used.

### Integration Time Increment Card (6F10.0) -

#### **DTMAX**

The maximum integration time increment which will be used for the equations of motion.

#### **DTMIN**

The minimum integration time increment allowed. If exceeded, the results will be written onto the restart tape, and the run will stop.

# SSF

The fraction of the sound speed transit time used for the integration time increment. It must be less than unity. Generally, SSF = 0.9 can be used, but some conditions (such as eroding interfaces) may require a lower value of SSF = 0.5.

**TMAX** 

The maximum time the problem is allowed to run. This time refers to the dynamic response of the system, not the central processor time (CPMAX) described next. The results at time = TMAX are written onto the restart tape, and the run is discontinued.

**CPMAX** 

= Central Processor time at which the results will be written onto the restart tape and the run will stop. This feature will be bypassed if CPMAX = 0. Time units are defined by subroutine CPCLCK.

**EMAX** 

= The upper limit for total kinetic energy if applied pressures are included (IPRES = 1 or 2). This is used for numerical instability checks. Run will stop if the kinetic energy exceeds EMAX. Leave blank if there are no applied pressures.

Pressure Cards for IPRES = 2 (615, F10.0) — These cards describe the applied pressures and the elements to which they are applied. If other pressures were used previously, they are all deleted, and the only applied pressures which act are those that are input in the current run. End with a blank card.

ELE1

The first element in a series of elements, to which pressure is applied. It must not be less than ELE1 or ELEN from a previous Pressure Card.

**ELEN** 

The last element in series of elements. It cannot be less than ELE1.

ELEINC

= The element number increment between ELE1 and ELEN. If ELE1 = 100, ELEN = 120 and ELEINC = 5, then pressures are applied to elements 100, 105, 110, 115, 120.

N1

= The node number opposite the triangular face of element ELE1 to which the pressure is applied.

NN

= The node number opposite the triangular face of element ELEN to which the pressure is applied.

NODINC

The node number increment between N1 and NN. For the elements described under ELE INC (100, 105, 110, 115, 120), if N1 = 200, NN = 208 and NODE INC = 2, then the pressures are applied to the triangular faces opposite nodes, 200, 202, 204, 206, 208, of elements 100, 105, 110, 115, 120.

PRES

= The pressures which are applied to the triangular faces of the elements described on this card (force/area).

Time-Pressure Cards for IPRES = 2(2F10.0) - These cards allow the applied pressures to be varied as a function of time. A minimum of two cards must be used, which

span the time from the beginning of the run to TMAX. Program currently dimensioned for a maximum of 50 cards. End with a blank card.

PTIME = The time corresponding to P(T). Cards must be input in order of increasing time.

The factor by which all pressures are multiplied at the corresponding time. Intermediate values are linearly interpolated between values at specified times.

Change Card for CHANG = 1 or 2 (F10.0, 1015) — This card is used only if changes are to be made which reduce the size of the problem. The portions of the problem which remain are those which were input first. Common uses are to drop the explosive gases after a liner has been accelerated, or to drop the target after a projectile has perforated the target. For CHANG = 1 the problem size is reduced only and there are no expansions. For CHANGE = 2 there will be problem expansions as well as problem reductions.

TDROP = Time at which change occurs.

P(T)

NODE = Total number of nodes which remain in the revised problem.

PNODE = Number of projectile nodes which remain in the revised problem.

ELE = Total number of elements which remain in the revised problem.

PELE = Number of projectile elements which remain in the revised

NSLID = Number of sliding surfaces which remain in the revised problem.

NPLOT = Number of nodes for which time-history data are written, which remain in the revised problem.

LPLOT = Number of elements for which time-history data are written, which remain in the revised problem.

NFAIL = Number of elements which will be designated to fail totally.

This type of failure sets all stresses in the element to zero. It essentially makes the element disappear except that mass is retained at the nodes.

NAB = Total number of NABOR nodes which remain in the revised problem.

PNAB = Number of projectile NABOR nodes which remain in the revised problem.

Designated Element Failure Card for NFAIL > 0 (1615) - This card is used only if there are elements to be totally failed.

**EF1 ... EFN** 

= Elements to be totally failed in the revised problem.

Change Add Card for CHANG = 2 or 3 (F10.0,615) - This card is used only if there are additions to be made to the problem. These additions can be made in conjunction with previous problem reductions (CHANG = 2) or they can be made to the original problem (CHANG = 3).

**TADD** 

= Time at which the change (problem size expansion) occurs.

**NSLID** 

= Number of sliding surfaces in the expanded problem. If this is greater than the existing numbers of sliding surfaces, the program will read input data for the additional sliding surfaces.

**XYZRIG** 

= Code to allow for rigid frictionless surfaces on positive sides of planes at x=0, y=0 and/or z=0. See description given in the Miscellaneous Card in the Preprocessor. It must be input here even if input in the Preprocessor

SPLIT

= 0 or 1. See description given in the Miscellaneous Card in the Preprocessor.

N1R, NNR

= First and last rigid body nodes as described in the Miscellaneous Card in the Preprocessor. They must be input here even if input in the Preprocessor.

N1L, NOR, NIR, NPL = Node geometry descriptions if internal loads are desired. See description given in the Miscellaneous Card in the Preprocessor. They must be input here even if input in the Preprocessor.

**NRST** 

Number of groups of nodes to have restraints redefined.

0 will not print any node or element data

1 will print data for all nodes and elements

**IPRINT** 

2 will print data for all nodes at y=0 and all elements with one face at y=0

3 will print data for all added nodes and elements

4 will print data for all added nodes at y=0 and all added ele- $\bigcup$  ments with one face at y=0

Target Scale/Shift/Rotate Card for CHANG=2 or 3 (F10.0) - This card is the same as used in Preprocessor. Applied to added target nodes only in the expanded problem. Must be included even if there are no additional nodes to be input.

Additional Target Node Data for CHANG=2 or 3 — These cards are required to define the additional nodes (for target only) for the expanded problem. Same format as used in Preprocessor. End with a blank card. Include blank card even if there are no additional target nodes.

Additional Target Element Data for CHANG=2 or 3— These cards are required to define the additional elements (for target only) for lthe expanded problem. Same format as used in the Preprocessor. End with a blank card. Include blank card even if there are no additional target elements.

NSLID, NRST data read as required. Same format as used in Preprocessor.

Target Velocity Card for CHANG=2 or 3 (30X, 3F10.0) – This card defines the nodal velocities of added target nodes only in the expanded problem. See descriptions for Velocity/Detonation Card in Preprocessor. Must be included even if there are no target nodes or if no additional target nodes were input. If there are no target velocities, do not leave the card blank. Instead, input velocities as 0. Must be followed by a blank card.

#### Plot Card (515, 5X, 4F10.0) -

CYCLE	=	Same restart cycle as specified on the Identification Card.
SYS		0 will not write the system data on the Plot Tape.
313		1 will write all the system data on the Plot Tape.
		0 will not write the internal loads data on the Plot Tape.
LOAD	=<	1 will write all the internal loads data on the Plot Tape.
		This option can only be used if N1L, NOR, NIR and NPL are properly defined in the Preprocessor Miscellaneous Card.
NPLOT	=	The number of nodes whose data will be written on the Plot Tape. The individual nodes are specified on the Designated Nodes Cards.
LPLOT	=	The number of elements whose data will be written on the Plot Tape. The individual elements are specified on the Designated Elements Cards.
DT SYS	=	The time increment at which the System and Internal Loads data are written on the Plot Tape (time). These quantities do not vary as rapidly as do the individual node and element data so a larger time increment can be used.
TSYS	=	The time at which the first System and Internal loads data are written on the Plot Tape. If left blank, the time at the beginning of the Main Routine run will be used (time).
DT NODE	=	The time increment at which the Individual Node and Element data are written on the Plot Tape (time). These quan-

tities vary more rapidly than the System and Internal Loads data so a smaller time increment can be used.

**TNODE** 

The time at which the first Individual Node and Element data are written on the Plot Tape (time).

**Designated Nodes Cards (1615)** – This card is used only if there are node data to be written on the plot tape (NPLOT > 0 on the plot card).

N1 ... NN

Individual node numbers whose data will be written on the Plot Tape. They must be in ascending order.

**Designated Elements Cards (1615)** — This card is used only if there are element data to be written on the plot tape (LPLOT > 0 on the plot card).

E1 ... EN

= Individual element numbers whose data will be written on the Plot Tape. They must be in ascending order.

Data Output Cards (2F10.0, 3I5) — These cards are used to specify various forms of output data at selected times, and the last card must be for a time greater than TMAX even though output will not be provided for that specific time. Recall that output is automatically provided at TMAX and a data output card need not be provided for this time. End run with a blank card.

TIME

= Time at which output will be provided.

**ECHECK** 

- A code which governs the printed output. Three options are provided:
  - (1) If ECHECK is greater than 1000, the individual node and element data will not be printed. Only system data such as centers of gravity, energies, momenta, and net velocities are provided for the projectile, target, and total system.
  - (2) If ECHECK = 999, system data will be printed as will nodal data on the plane of symmetry at y=0. Element data will not be printed.
  - (3) If ECHECK is less than 999, the system data and individual node data will be printed. Individual element data will be printed for all elements which have an equivalent plastic strain equal to or greater than ECHECK. For example, if ECHECK = 0, all element data will be printed. If ECHECK = 0.5, only those elements with equivalent plastic strains equal to or greater than 0.5 will have data printed.

NOTE: There are some instances when data are printed even though not specified with a data output card. If the min-

imum time increment, DTMIN, is violated, or the specified central processor time, CPMAX, is exceeded, or the maximum run time, TMAX, is achieved, the results are written on the restart tape. The value of ECHECK used for the printed output is that value which is on the following data output card.

0 will not print internal loads data.

LOAD 1 will print internal loads in a slender projectile. This option can only be used if N1L, NOR, NIR and NPL are properly

defined in the Preprocessor Miscellaneous Card.

0 will not write results on the restart tape.

1 will write results on the restart tape.

**YPRINT** 1 will restrict printing for node data to nodes with y=0, and

to element data to elements with one face on the y=0 plane and an equivalent plastic strain equal to or greater than

ECHECK.

#### 3. INPUT DATA FOR THE POSTPROCESSOR

The function of the Postprocessor is to provide plots of the results in the form of state plots and time plots. The state plots show results for the entire system at a specified time and the time plots show results for a specified variable as a function of time.

It is possible to interject user comments into the data by use of a \$ character, as described for the Preprocessor.

#### a. State Plots

See September 1. Control of the Cont

SAVE

Input data for state plots are summarized in Figure 6. The first group of data is for geometry plots, velocity vector plots and contour plots of eight different variables. These cards should be input in order of increasing cycle numbers. This first group of cards (Geometry, Velocity, Contour) is ended with a blank card.

The second group of cards is for internal loads in a slender projectile. These should also be input in order of increasing cycle numbers and ended with a blank card.

# Geometry Plot Card (215, F10.0, 212, 4X, 212, 18X, A30) -

= Code to specify geometry plot. 1

= Cycle number of the plot which is desired. The cycle numbers of **CYCLE** the data written on the restart tape are given in the printed output of the Preprocessor and the Main Routine. If CYCLE = 0, the plots are requested on the basis of time.

TIME

Time of the plot which is desired. Plots can be requested by either TIME or CYCLE.

O will use the axes from the previous plot. This option allows deformed geometry to be plotted together with contours or velocity vectors, for instance. The previous VIEW is used.

**AXES** 

1 will automatically compute the axes to include all nodes. The vertical axis is specified to be 10 units, and the horizontal axis is 13 units, using the same scale as the vertical axis. When VIEW = 5, 6, 7, then the median of the Y, X, Z span is used for the cutting plane.

2 will read the coordinate limits of the plot.

**VIEW** 

A code to specify the view requested. VIEW = 1, 2, 3 requests two dimensional plots of the x-z, y-z and x-y axes respectively. VIEW = 4 requests a three-dimensional plot. VIEW = 5, 6, 7 requests cutting plane plots with the cutting plane parallel to the x-z, y-z, and x-y planes respectively. VIEW = 8 requests a cutting plane plot using an arbitrarily positioned cutting plane.

FAIL

= 1 will place an "x" at the center of each fractured (partially failed) element face for VIEW = 1, 2, 3, only. Otherwise leave blank.

MATL

0 will draw all materials.

N will draw only elements with material number N.

TITLE

A title which is printed on the plot.

Plot Limits Card for AXES = 2 (6F10.0) - This card specifies the portion of the problem which is plotted. Regions beyond those specified are not plotted. For the two-dimensional plots, the vertical axis is 10 inches long, and the horizontal axis is as specified. The length of the horizontal axis will vary since it has the same scale as the vertical axis. The vertical axes are the z axis (VIEW = 1 and 2) and the y axis (VIEW = 3). For the three-dimensional plots, the axes are scaled such that the entire region is included within the 10-inch vertical axis and a 13-inch horizontal axis.

**XMAX** 

= The maximum x coordinate included in the plot (length). When VIEW = 6, XMAX is the position of the cutting plane.

**XMIN** 

= The minimum x coordinate included in the plot

**YMAX** 

The maximum y coordinate included in the plot. When VIEW = 5, YMAX is the position of the cutting plane.

**YMIN** 

= The minimum y coordinate included in the plot

**ZMAX** 

The maximum z coordinate included in the plot. When VIEW = 7.
ZMAX is the position of the cutting plane.

**ZMIN** 

The minimum z coordinate included in the plot.

**LMAX** 

The maximum element number included in the plot. If both LMAX and LMIN are blank or zero, then all elements are plotted.

**LMIN** 

- The minimum element number included in the plot.

3D Perspective Card for VIEW = 4 or 8 (8F10.0, I5) - This card is included only for the 3D plots and arbitrarily oriented cutting plane plots.

XEYE, YEYE ZEYE = Coordinates of the observer (length).

XPLANE,

XPLANE, YPLANE, ZPLANE Coordinates included in the plane on which the results are plotted for VIEW = 4. The plane is normal to a line from XEYE, YEYE, ZEYE to XPLANE, YPLANE, ZPLANE. For VIEW = 8, this plane is the cutting plane.

0 will plot all free surfaces (no hidden lines)

LHIDE

= < 1 will plot only surfaces which are visible to the observer. This option can require significant CPU time, especially if the nodes are not memory contained.

2 will produce two plots, one each with LHIDE = 0 and LHIDE =

LHIDE is not used for VIEW = 8.

Velocity Vector Plot Card (615, F16.6, 5A6) — Only previously undefined variables are defined. See Geometry Plot Card description for others. Cutting planes, VIEW = 5, 6, 7, or 8, are not implemented for velocity plots.

2

= Code to specify velocity vector plot.

0 will draw all element faces.

**EDGE** 

| < 1 will plot only an outline around the external surfaces for VIEW = 1, 2, 3. Otherwise leave blank.

ARROW

= 1 will place arrowheads on the velocity vectors.

**VSCALE** 

= The velocity that will give a velocity vector with a length of 10 using the scale of the plot. If left blank, VSCALE will be determined to give the longest vector a length of two percent of the length of the vertical axis.

Plot Limits Card for AXES = 2(6F10.0) - This is the same as described for Geometry Plots.

3D Perspective Card for VIEW = 4 (6P10.0) - This is the same as described for Geometry Plots except hidden line option is not allowed

Contour Plot Card (615, 10X, 5A6, 215) — This card requests contour plots of element variables. Contours are determined by first computing the variable quantities at the nodes (i.e., the nodal pressure is the average of the pressures of all elements which contain the node). Then the contours are drawn through the nodal quantities. The card is mostly used for two-dimensional plots, (VIEW = 1, 2, 3). The 3D plots have the contours drawn only on the element faces. Only previously undefined variables are defined. See Geometry and Velocity Plot Cards for others. Cutting planes, VIEW = 5, 6, 7, or 8, are not implemented.

**TYPE** 

= A code to specify which variable is requested. See Figure 6 for description of variables.

**NLINE** 

Number of contours to be plotted. Currently limited to 8. If NLINE = 0, six contours will be plotted at values of 5, 20, 40, 60, 80 and 95 percent of the range between the minimum and maximum variable quantity limits.

SYMBOL

Increment at which symbols are placed on contour lines. SYMBOL = 1 will place symbols at the forward end of each contour line within an element, and SYMBOL = 5 will place symbols at the forward end of every fifth element, etc. SYMBOL = 0 will not put any symbols on the contour lines.

**PRINT** 

= 1 will print the nodal quantities of the specified variable. Otherwise leave blank.

Plot Limits Card for AXES = 2 (6F10.0) - This is the same as specified for the Geometry Plot Card.

Contour Specification Card (8F10.0) - This card is required only for NLINE > 0.

VAR(I)

Magnitude of contours to be plotted (I = 1, NLINE).

Internal Loads Plot Card (15, 5X, 215, 2X, 311, 15X, 5A6 — This card requests plots of internal loads. The data must have been previously generated in a Main Routine run by setting LOAD = 1 on the Plot Card. Sign conventions for the internal loads are given in Figure 20. The loads are only for one-half the rod since a plane of symmetry is used in the geometry generators.

15

Code which specifies internal loads plots.

CYCLE

The cycle number of the plot which is desired. The cycle numbers of the data written on the plot tape are given in the printed output of the Main Routine. If CYCLE = 0, the plots are requested on the basis of time.

TIME

 Time of plot which is desired. Plots can be requested by either TIME or CYCLE. 1 will automatically scale axes to include all extreme data points.

2 will allow coordinate axes limits to be specified.

IP = 1 will give plots of axial loads. Otherwise leave blank.

IV = 1 will give plot of shear loads.

IM = 1 will give plot of bending moments.

TITLE = A title which will be written on the plot.

Plot Limits Card for AXES = 2 (7F10.0) -

PMAX = Maximum coordinate of vertical axial load axis (force).

PMIN = Minimum coordinate of vertical axial load axis.

VMAX = Maximum coordinate of vertical shear load axis (force).

VMIN = Minimum coordinate of vertical shear load axis.

BMAX = Maximum coordinate of vertical bending moment axis (force-dis-

tance).

BMIM = Minimum coordinate of vertical bending moment axis.

LENGTH = Maximum coordinate of horizontal axis, which is defined as the deformed centerline distance from the free end of the rod (length).

### b. Time Plots

Input data for time plots are summarized in Figure 7. System Plot Cards should be input first, followed by the Internal Loads, Individual Node and Individual Element Plot Cards. The variables are plotted as a function of time. The plot axes are divided into ten units each. End with a blank card.

System Plot Cards (215, 5X, F5.0, 4F10.0, A20) — These cards request plots of the system variables. Each plot contains data for the projectile, the target and the total system (projectile plus target). These data must have been previously written on the plot tape by setting SYS = 1 on the Plot Card in the main Routine.

TYPE = A code describing the type of plot. See Figure 7 for description of type. It must be in range of 1-26.

0 will automatically select coordinates to include maximum and minimum values of variable for total duration of time.

AXES = 1 will read the coordinate limits of the plot.

SCALE = Factor by which the variables are multiplied before plotting.

TMAX = Maximum time included on horizontal axis if AXES = 1 (time).

TMIN = Minimum time included on horizontal axis if AXES = 1 (time).

VMAX = Maximum variable included in vertical axis if AXES = 1.

VMIN = Minimum variable included on vertical axis if AXES = 1.

TITLE = A title written on the plot.

Internal Loads Plot Cards (315, F5.0, 4F10.0, A20) — These cards request plots of internal loads at a specified location in the slender projectile. These data must have been previously written on the plot tape by setting LOAD = 1 on the plot card in the Main Routine. Only previously undefined variables are defined. See System Plot Cards description for others.

27 will plot axial loads.

TYPE = 28 will plot shear loads.

29 will plot bending moments.

LAYER = The layer of lements at which the loads are plotted. Layer I is midway between node planes I-1 and I where node plane 1 is at the free end of the projectile.

Individual Node Plot Cards (315, F5.0, 4F10.0, A20) — These cards request plots of nodal variables. These data must have been previously written on the plot tape by specifying the requested nodes on the Designated Nodes Card in the Main Routine. Only previously undefined variables are defined.

**TYPE** 

A code describing the type of plot. See Figure 7 for description of types. It must be in the range of 30-39. Note that acceleration data (TYPE = 36-38) may be incorrect for sliding surface and rigid body nodes.

NODE

= Specific node for which plot data are requested.

Individual Element Plot Cards (315, F5.0, 4F10.0, 3A6) — These cards request plots of element variables. These data must have been previously written on the plot tape by specifying the requested elements on the Designated Elements Cards in the Main Routine. Only previously undefined variables are defined.

TYPE

A code describing the type of plot. See Figure 7 for description of types. It must be in the range of 40-53.

ELE

= The specified element for which plot data are requested.

### 4. PROGRAM STRUCTURE AND FILE DESIGNATION

EPIC-3 consists of four FORTRAN-77 programs, PREP, MAIN, POST1, and POST2. The Preprocessor, PREP, converts the information given in the input data into the form used in a restart file and writes a restart file. The Main Routine, MAIN, reads a restart file, advances the simulation for some time cycles, and writes both a new restart file and plot files at user requested simulation times. The Main Routine can read any restart file (PREP or MAIN), which allows the simulations to be carried out in several smaller runs or one larger run. The Postprocessor for state plots, POST1, produces plots which show the state of the simulation at a given simulation time. POST1 can read restart files to produce geometry, velocity vector, and contour plots. POST1 can also read the plot data file to produce internal loads plots. The Postprocessor for time plots, POST2, produces plots which show how simulated quantities change during the simulation time. POST2 reads the plot data file. The user must request MAIN to write the proper data into the plot data file so that POST2 will have the appropriate data available. The hierarchy charts for the four programs are given in Figures 21-24 and subroutine groupings are given in Tables 1 and 2. Additional background on program structure is given in References 2 and 9.

All the files used by EPIC-3 are defined in COMMON/FILES/ except for two scratch files used by POST1. The common block is assigned values by assignment statements at the beginning of each program. The current designation and descriptions are:

IN	=	5	Input file for all programs
IOUT	=	6	Output file for all programs
ITAPIN	=	9	Restart file input read by MAIN and POST1
ITAPOT	=	10	Restart file output written by PREP and MAIN
NFILER NFILEW	=	1 > 2 >	Node Scratch file pair used for out of memory problems by PREP, MAIN, POST1
LFILER LFILER	=	3 4	Element scratch file pair used for out of memory problems by PREP, MAIN, POST 1
ISFILR	=	8	Sliding surface scratch file used by PREP, MAIN, POST1
ISFILW	=	14	Sliding surface scratch file used by MAIN
ITAPLT	=	7	Plot data file written by MAIN and read by POST1 and POST2
IPLTIN	=	13	Plot data file read by MAIN
ITGAD	=	11	Target addition scratch file used by MAIN

Files 1, 2, 3, 4, 8, 11, and 14 are opened as FORTRAN-77 nameless scratch files when needed.

The unit 1 is also used by PREP and MAIN. The input file on channel IN is stripped of comments and written to file TEMP.DAT on channel 1. Then TEMP. DAT is used for input on channel IN. TEMP. DAT is deleted on normal program completion.

POST1 uses two additional scratch files.

TABLE 1. SUBROUTINE GROUPINGS FOR EPIC-3 CODE

PREP	MAIN1	MAIN2	GEN	NABOR	POST1	SUBS	POST2
PREP	MAIN	MATCH	BRICK	CRUSH3	POST1	CPCLCK	POST2
GEOM	ASTRES	MIEGRU	ECORE	INVAQ	ARROW	ERAFLG	EPLOT
MATL	CHANGE	MOTION	EGEOM	MEGRU3	AUTOS	EREAD	ILPLOT
MATLIB	CRUSH	MOVE	ENOSE	NABOR3	CTOUR	EREAD1	NPLOT
START	DAMAGE	MSERA	ENPLAT	SEARCH	CVALUS	EREAD2	PDATA
	EGET	MSTEST	EPLATE	STRES3	DATSET	ERTAPE	READTP
	ELOOP	MTMP2	EROD		EDGE	EWRITE	SYPLOT
1	EPLOTS	NLOOP	ESPHER		GEOM2	EWTAPE	
1	EPUT	NPLOTS	MASS		GEOM3	HDATA	
	EQSTS	ORIENT	MSFLAG		GETCON	LBPOS	
	ERODE	PAVE	NBCORE		GPLOT	LPOS	
	EULER	PCALL	NBLINE		HCHECK	MSNEW	
	FIND	PREAD	NCORE		HIDEL	NBPOS	
}	FORCE	REPORT	NGEOM		ILOADS	NFIX	
	FSGRAD	RIGID	NLINE		LOADP	NPOS	
	GCON	ROTOF	NNBRIK		PLINE	NREAD	
1	HEBURN	SEEK	NNOSE		PRTCON	NREAD1	
	ISTRES	SLIDE	NNPLAT		SETORG	NREAD2	
	LOAD	STHARD	NPLATE		(PERSPC)	NRTAPE	
		STRAIN	NROD		SETUP	NWRITE	
		STRESS	NSPHER		SORT2	NWTAPE	
		SYMINV	RGEOM		SORT3	RECALL	
		SYMOR	SCYLN		VPLOT	SAVE	
ļ	·	TARGAD	SDISK	i		SDATA	
		TCHECK	SGEOM			SETFLG	
		TRNST	SIZE			SWITCH	
		VOLUME	SLAVEN				
			SNNEW	,			
			SNOSE				
	]		SPLATE				
		i	SSEK2				
	ļ	l	TETRA				
[			WEDGE1		}		
1 1			WEDGE2				
			WRITEG				

N20-010.JF

TABLE 2. REQUIRED GROUPS OF SUBROUTINES FOR VARIOUS TYPES OF RUNS

TYPE OF RUN	REQUIRED SOUBROUTINE GROUPS										
TYPE OF RUN	PREP	MAIN1	MAIN2	GEN	NABOR	POST1	SUBS	POST2			
PREPROCESSOR	×			×			×				
MAIN ROUTINE (NO NABOR NODES)		×	×	×			×				
MAIN ROUNTINE (WITH NABOR NODES)		×	×	×	×		×				
STATE PLOTS						×	×				
TIME PLOTS								×			

### 5. OPTIONS FOR MEMORY CONTAINMENT OF DATA

EPIC-3 can simulate problems that are represented by a number of nodes and elements small enough to fit into the node and element arrays, But EPIC-3 can also simulate problems whose representation exceed the capacity of the arrays. This capability is achieved by using a primitive paging scheme. Pages of nodes or elements can be shuffled between arrays and files. The price of using this large problem capability is a slight increase in CPU time and a large amount of file access time. On a typical modern computer the file access time for out of memory elements roughly equals the CPU time. The file access time for out of memory nodes will usually be less because there usually are fewer nodes than elements. When both nodes and elements are out memory, then the file accesses are synchronized so that the file access times add together. A notable exception is in POST1 when producing hidden line geometry plots. The hidden line algorithm requires the comparison of every node with each exterior element face. A significant number of passes through the node file may be required for one picture. The most efficient way to run a simulation is with large enough array sites (nodes and elements) so that the problem is contained in memory. Even virtual memory systems are faster than the EPIC-3 out of memory option. This version of EPIC-3 has been written to allow array size changes to be made easily.

The node and element arrays in EPIC-3 are not treated as single arrays but are broken into convenient chunks called blocks. The paging scheme explained in the preceding paragraphs requries pages smaller than the array size. The page size is one block. The vectorization of element calculations imposes a block size because of the vectorization characteristic of computers and the corresponding temporary arrays which are needed. The node and element blocks can be chosen to be different sizes. In both cases (node and element) the array sizes should be a multiple of the corresponding block size.

The number of element blocks needed for array containment is printed by PREP after the element input data section. Since there is no penalty for more element blocks than needed for array containment, a series of problems can all be run with a version of MAIN large enough to contain the largest problem. PREP executes quickly so there is no big advantage to array containment of elements but it is convenient to have PREP arrays the same size as MAIN. PREP will never stop because of problems with element blocks.

Choosing the number of node blocks to use is more complex when a small node array size is desirable. The minimum number of node blocks required is printed by PREP under the heading "Bandwidth Requirements for Main Routine". If PREP does not contain this number of node blocks it will stop at that point. MAIN also requires the minimum number of node blocks.

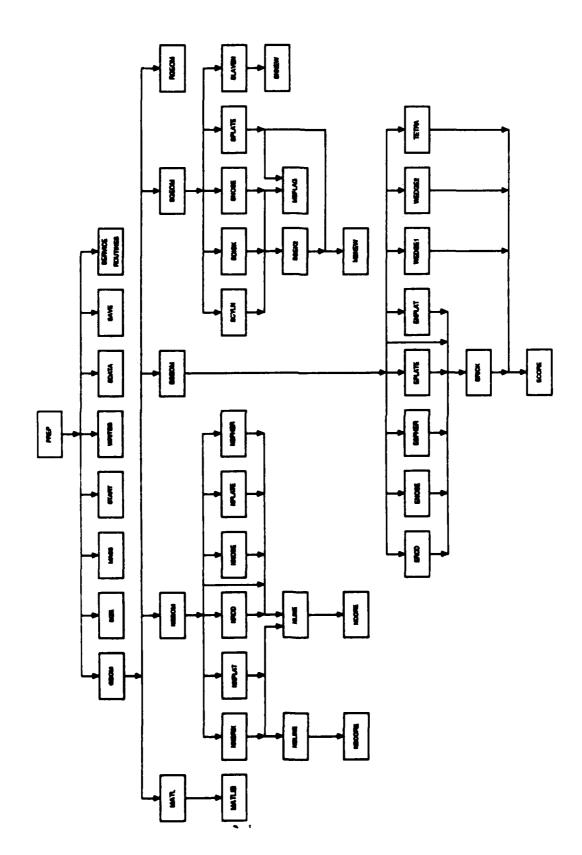


Figure 21. Hierarchy Chart for the Preprocessor

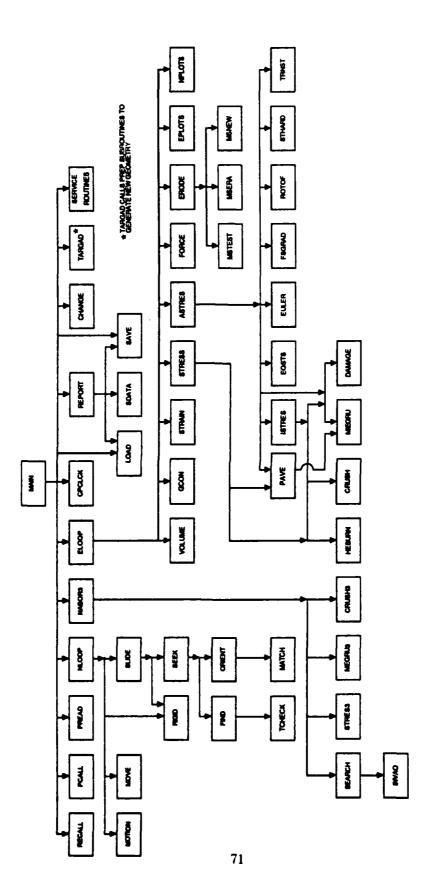


Figure 22. Hierarchy Chart for the Main Routine

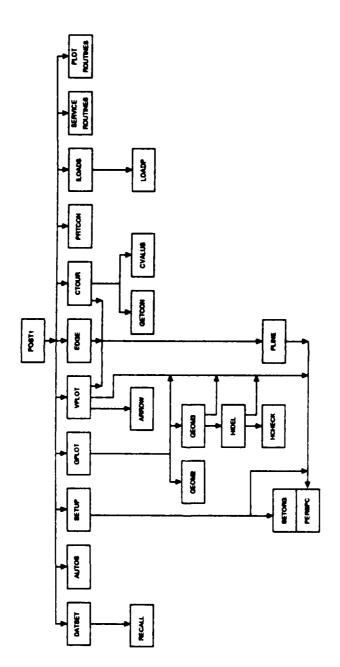


Figure 23. Hierarchy Chart for the State Plots Postprocessor

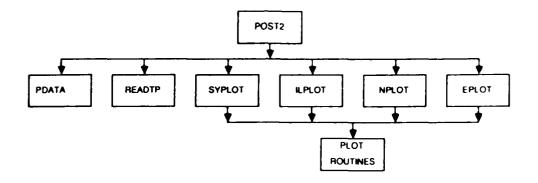


Figure 24. Hierarchy Chart for the Time Plots Postprocessor

Eroding slide surfaces pose a problem for the smallest number of node blocks required If NLAST, the largest node number on an eroding master surface at any time, is known then an accurate node block number can be given. An overestimate of NLAST will overestimate the node block number. If NLAST is not known and zero given, then an underestimate of node blocks will be given by PREP, and MAIN will dynamically check as the erosion happens. When the number of node blocks needed exceeds the number available, then MAIN stops. There is no advantage to having more than the minimum number of node blocks until the number sufficient for array containment is reached

### 6. INSTRUCTIONS FOR CHANGING PROGRAM DIMENSIONS

The COMMON declarations have been implemented in VAX style INCLUDE files. Unfortunately, this is not part of the FORTRAN-77 standards, but every mainframe system has a similar extension. This method allows all COMMON declarations to be the same because they all are copies of the same file. The labeled COMMON block ELEMNT' uses the PARAMETER MAXL to declare the size of the element arrays. The elements are handled in blocks of size LBSIZE. Currently LBSIZE is set to 60 in PREP. Only complete blocks can be used so a partial block at the end of arrays will be unused The smallest declaration for all elements in memory is to set MAXL equal to the small lest multiple of LBSIZE, which is equal to or larger than the number of elements. Only MAXL needs to be changed to change the number of elements. After MAXL has been changed, all the programs except POST2 should be recomposed and linked. Each program will automatically switch to out of memory mode when reeded. The element array sizes in the various programs (PREP, MAIN, POST1, do not need to be coor dirated, but the subroutine packages GEN and SUBS must have the same size COM MON blocks as the main program they are being linked to. The simplest thing to do is touse the same element array size everywhere. Similar considerations apply to nodes. The COMMON block is 'NODE, with PARAMETER MAXN. The node block size is NBSIZE which is set to 64 in PREP

The block sizes have been chosen carefully. The CRAY 1, which can vectorize this code, had a limit of 64 elements in a quick vector loop, so this sets an upper limit on the block size. The technique for pressure averaging in bricks requires that all 6 elements be present together in a block, so element blocks must be a multiple of 6. The existing element block size of 60 is the largest multiple of 6 equal to or less than 64. The array storage used to assist the vectorizing method in element loops must be coordinated with the element block size. The PARAMETER MAXV used in COMMON/VECTOR/ must be equal to or larger than LBSIZE. The element and node block sizes, LBSIZE and NBSIZE, are set in the opening code of PREP. This is the only place they are set. They are used to define the format of the restart files, so they are included in the restart file. MAIN and POST1 read LBSIZE and NBSIZE from the restart file.

The array storage used to assist reading and writing node and element blocks must also be coordinated with block sizes. The element buffering arrays are contained in COM-MON/EBUF/. The minimum array sizes needed are PIEB=3+(LBSIZE\*6) and PREB=LBSIZE\*25. The node buffering arrays are contained in COMMON/NBUF/. The minimum array sizes needed are PINB=2+NBSIZE and PRNB=NBSIZE\*17.

### 7. EXAMPLE PROBLEM

Preprocessor and Main Routine input data for a tungsten projectile impacting a steel target are given in Figure 25. The geometry of the computed response is shown in Figure 26 and output data are shown in Figure 27.

OBLIQU	E IMP	ACT OF	TUN	GSTEN RO	ONTO	STEEL	PLATE					
ī	0	1	1		0	0	1	2	0 :	39	0 0	I
11	0	1	1	1.0 1.	5							
9	0	1	1	1.0 999	•							
,	1.0		1.0	1.	)	0.0	0.	18	-45	. 0		
2 2	0	39	0	5.	1	0.25	1	. 0				
	0.25	3,	0.0	0.2		0.0	•					
3 2			•••	• • • • • • • • • • • • • • • • • • • •								
2	0	2	0	0.2	5	0.0	0.	25	0 .	. 0		
	1.0		1.0	1.	)							
4	1											
39	20	5	8	8		1.3	0.33			. 3	0.6667	1.0
	-4.5		0.0	0.	)	4.5	•	. 5	-0.	. >		
2												
2 2 3 2	1	38	1	11								
3	_		_									
2	1	0	586	11								
4 38	1 19	4	616	9								
30	1,9	•	010	,								
1	4	1	623	301 61	315	0	0	0	0.	. 0	80000.0	1.5
1 25	13	1	39	1 373								
	0.0		0.0	0.		0.0	•					
417	58.0		0.0	-41758.	J	0.0	0	. 0	0.	. 0	0.0000001	

OBLIQUE I	MPACT OF	TUN	GSTEN	ROD	ONTO	Steel	
3	0 0	1	0	0		0.0	5.0E6
1.	0 1.0	E-9		0.9	0.1	55-3	6.0
0.7E-	4 615	615	1920	1920			
0							
0.1E-	4 100	0.1	0	1	1		
0.28-		0.1	Ō	ī	ī		
0.38-	4 100		Ŏ	ī	ī		
	4 100		ŏ	ī	ī		
	4 100		ŏ	ī	ī		
	4 100		ŏ	ī	ī		
	4 111		ŏ	ī	ī		
	4 100		ŏ	ī	ī		
	4 100		ŏ	i	ī		
	3 100		ŏ	î	î		
0.118-		0.1	ŏ	i	î		
	3 100		ŏ	î	ī		
	3 100		ŏ	•	•		
0.148-		0.1	ŏ	•	- 1		
			ŏ	- 1	- 1		
0.1E-	V	0.1	U	Τ.	1		

Figure 25. Input Data for the Example Problem

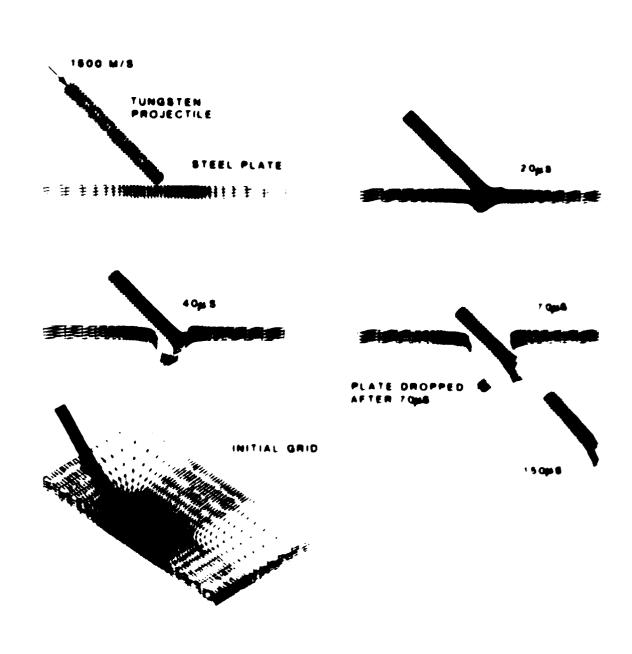


Figure 26 Computed Response of Example Problem

```
ASE TUMBER - 1
Y LE - 670
TIME - 7002/13E-04
TIME 0.157050E 06
P TIME NOVES - 294707E-01
UTPUT ODE EIMERS - 1,000010E+04
TAPE (DE 18AVE - 1
```

SUMMADE OF SYSTEM DATA FIRE Y LE ... 670 AT TIME + ... 5 TOGETSE 04

		PROJECTILE	TAPGET	TOTAL SYSTEM
#A3:		. 1444328 63	5 .40230E 01	0 155494E 6.
を扱いたまた 明みシン	•	1 . 62760E 03	0 .410768 01	0 301354E 01
一時に明を開する 「アー丁製造物でした」みかってで、水、人名とも	_	_ *36 "G98 G3	60 6 5 9 8 9 1	0 2990258 0.
- 特の何を留する - P 「信息会でした Addis マード Addis	•	1 1549078 61	5 .01 se 2E + 60	0 1039338.00
MOMENTS OF IMERTIA ABOUT 2 ARIS	•	. 5144198 63	1363108+00	0 1305038+00
TITAL EBERGIES			6 .51481E+04	0 1244442.0
e:mer: enemoits		. 5 5 3 1 8 2 • 6	9 394 7658 - 65	0 1092658+0
WTERMAL ENERGIES	•	5 59+159E+65	0-11/01/8+64	0 1717878+04
P1 257. #088		. 1543978+05	. 9362**E+65	0 1292678+06
maximim v v v Potanti		5154542+61	509922.01	6 535454E+6.
MINITED W. F. JOHNSONSTEE	-	/ 9.8 11 4E+6	6 456.578+61	0 450157E+C.
MARIMUR - SOBBIBATES	-	. 3C##1GE+G:	9 4509648+0.	0 4509048+6.
HIBINUM - GUBBINATES	•	6 50.451E 01	0 .000008 • C C	0 5014518 6
MARIMUM : GOBETBATES	•	6 262754E+61	5 84.9248 CZ	0 102754E+0.
RIMIRUM t COBCINATES	•	U 25.0978+Qs	6 2533692.62	0 2513898+0;
n r bipt Tion		1 1699952.00	9 1101268 61	0 477807E 6:
. The bulgetfion	-	5 13.332E+60	0 1193698 + 61	0 2151338+0.
. # 1 SIBELTION	•	0 444212E+00	0 1477448+00	0 2857956.00
<b>医食品质 网络网络银宝木 「京」まり510年(715日</b>		1 /65/48E+0.	5 4642248+6.	G 3116898+G2
物を高か、時の時を提する。(新二) しょかまくてもつか	•	- 456052R+UC	0 1000138 + 01	0 6240448.GC
: HEAD MOREPTA IN 1 LIPE-TION	•	C 2631048+02	0 4951048-01	0 311694E.G.
. me we like the transfer of the control of the con		. 15510.2.65	5 3.31778.63	0 2601918.0.
HEAR OLD STIRS IN 1 CIDE: TION	•	0 6.69754.63	U 1286 48+02	0 4008278.02
MEAN RELACITIES IN C DIRECTION	•	C 1513498+05	0 3340118+63	0 3001946+64
##* /#LSC 1718#	•	6 4997098+65	0 4636362+03	0 2831448+6+
AN. LAN MOMENTA ABOUT A & ARES		. 5150698.60	0 9818918.01	0 4299428+07
ARU LAR MOMERTA ABOUT 1 G ARES		5 .560178 + 01	0 401466E+00	0 743244E+01
ARU-LAS MOMENTA ABOUT I . ARES	•	C 433744E+0C	0 41494 TE - 01	0 5664398.02
AND LAP SELECTIES ABOUT A ARES			J 374495E+63	9 2104642.6.
THE CAP RESULTIES ABOUT IT IS ARES	•	0 2382598+04	/ 591184E+01	0 72,144E.U.
AND LAN VELCCITIES ABOUT E TO ARES	•	U-152480E+U3	9 168540E+02	0 4294448+01

FOLE . . . . S DATA MRITTER & FILE .C FOR RESTART OR POST PROCESSING

Figure 27 Output Data for the Example Problem

# SECTION III CONCLUSIONS AND RECOMMENDATIONS

User instructions have been provided for the EPIC-3 code. This code can be used for a wide range of problems involving high-velocity impact and explosive-metal interaction.

## REFERENCES

- Johnson, G.R. EPIC-3, A Computer Program for Elastic-Plastic Impact Calculations in Three Dimensions, Honeywell Inc., Hopkins, MN, Contract Report BRL CR 343, July 1977.
- 2. Johnson, G.R., D.D. Colby, and D.J. Vavrick. Further Development of the EPIC-3 Computer Program for Three-Dimensional Analysis of Intense Impulsive Loading, Honeywell Inc., Hopkins, MN, AFATL-TR-78-81, July 1978, Unlimited Distribution.
- 3. Johnson, G.R., and R.A. Stryk. *User Instructions for the EPIC-2 Code*, Honeywell Inc., Edina, MN, AFATL-TR-86-51, August 1986, Unlimited Distribution.
- 4. Johnson, G.R., and W.H. Cook. "A Constitutive Model and Data for Metals Subjected to Large Strains, High Strain Rates and High Temperatures," Proceedings of Seventh International Symposium on Ballistics. The Hague, The Netherlands, April 1983.
- Matuska, D.A., R.E. Durrett and J.J. Osborn. Hull User Guide for Three Dimensional Linking with EPIC-3. Orlando Technology, Inc., Shalimar, FL, ARBRL-CR-00484, July 1982.
- 6. Johnson, G.R., and W.H. Cook. "Fracture Characteristics of Three Metals Subjected to Various Strains, Strain Rates, Temperatures and Pressures," Engineering Fracture Mechanics, Vol. 21, no. 1 (1985).
- 7. Johnson, G.R. "Recent Developments and Analyses Associated with the EPIC-2 and EPIC-3 Codes." Advances in Aerospace and Structures and Materials. Edited by S.S. Wang and W.J. Renton. AD-01, ASME, 1981.
- 8. Johnson, G.R., and R.A. Stryk. "Eroding Interface and Improved Tetrahedral Element Algorithms for High Velocity Impact Computations in Three Dimensions," International Journal of Impact Engineering, Vol. 5 (to appear in 1987).
- 9. Johnson, G.R., D.D. Colby, and D.J. Vavrick. "Three-Dimensional Computer Code for Dynamic Response of Solids to Intense Impulsive Loads." *International Journal for Numerical Methods of Engineering*, 14, no. 12 (1979).
- 10. Johnson, G.R. "Dynamic Analysis of Explosive-Metal Interaction in Three Dimensions." *Journal of Applied Mechanics*, ASME, 103, no. 1 (March 1981)
- 11. Johnson, G.R., R.A. Stryk, and J.G. Dodd. "Dynamic Lagrangian Computations for Solids, With Variable Nodal Connectivity for Severe Distortions," International Journal of Numerical Methods in Engineering, Vol. 23 (1986).

*ያመያቸው የፌሚ*ኒቶ አለው (እር አይላር)

#